

Research and Modeling of Nonlinear Acoustic Processes in a Layered Nonlinear Medium with a Porous Fluid-Saturated Inclusion of a Hierarchical Type

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How to cite this paper: Hachay, O., Dryagin, V. and Khachay, A. (2019) Research and Modeling of Nonlinear Acoustic Processes in a Layered Nonlinear Medium with a Porous Fluid-Saturated Inclusion of a Hierarchical Type. *Open Journal of Geology*, 9, 497-506.

<https://doi.org/10.4236/ojg.2019.99032>

Received: August 2, 2019

Accepted: August 31, 2019

Published: September 3, 2019

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Abstract

Problem statement: The results of the study of seismic acoustic emission arising in a porous two-phase geological environment under acoustic influence are presented. Acoustic emission arising in reservoirs of oil fields using good observations is considered. The regularity of the emission processes of acoustic emission, which manifests itself in the form of discrete spectra of signals similar to oscillations of nonlinearly coupled oscillators, is shown. Spectra have special characteristics for each type of rock. **Applied method and design:** An algorithm for modeling the process of resonant acoustic response of a porous fluid-saturated reservoir with hierarchical structure and plastic properties on acoustic frequency excitation is developed. That algorithm is developed as an iterative process for the solution integral and integral-differential equations. The frequencies that are parameters of the direct problem are used from the spectra of observed data of acoustic emission in the oil wells. **Typical results:** For the first time, it had been found the relation between resonant frequencies of the acoustic emission and plastic properties, these values of frequencies had been used in the algorithm of modeling distribution of longitudinal waves in the fluid saturated nonlinear plastic environment. **Concluding note (Practical value/implications):** The analysis of these emission processes can serve as a source of information about the filtration-capacitive properties of productive reservoirs of a porous type with a hierarchical structure. It is used by practical data of oil fields of Western Siberia.

Keywords

Seismic Emission after Acoustic Impact, Reservoir of Hierarchical Structure

1. Introduction

Using the method of Acoustic emission (AE) research, it is possible to obtain information about the processes occurring inside the substance of the reservoir in the well. It has an important advantage over other geophysical methods due to its high resolution in the frequency range. For understanding processes in a saturated porous medium and building adequate models, it is not enough to take into account only the linear relationship between the AE and dynamic processes in the medium, which is a nonlinear system. The principal feature of a nonlinear medium is the interaction of a limited number of waves associated with the conditions of frequency resonance and wave vectors [1]. The study of acoustic emission in samples of sandstones of terrigenous reservoirs under the action of mechanical stresses was carried out at the UIK-AE core research unit [2]. The energy of the acoustic emission signal, which is released in the process of acoustic impact, was determined by the method of calculating the spectral energy density in the whole recorded frequency range from units of hertz to 20 kHz by the Intel Graph program. In accordance with the theory of nonlinear systems, when nonlinearly coupled oscillators interact, processes are possible when the system generates oscillations with combinational frequencies. In this case, the condition of resonance of frequencies is fulfilled and it is indicated that energy can be exchanged between oscillators, in which the energy of the excited high-frequency oscillator is transferred to two low-frequency oscillators or the reverse process, the merging of low-frequency oscillations. Such an interaction has, for example, a place in the system of three nonlinearly coupled oscillators described by a system of equations [1].

$$\ddot{x}_i + \omega_i^2 x_i = \mu \alpha_i x_j x_k; i = 1, 2, 3; j, k \neq i$$

For a small value of μ , this is a weakly nonlinear system. Its behavior is close to the superposition of quasiharmonic oscillations of oscillators with slowly varying amplitudes. Due to the nonlinear coupling, oscillations of two oscillators with frequencies ω_1 and ω_2 generate oscillations with a combination of frequencies ω_1 and ω_2 in the system. The action of a small nonlinearity accumulates if the frequency resonance condition is fulfilled:

$$\omega_1 + \omega_2 = \omega_3$$

When sandstone is deformed, which is an inhomogeneous medium characteristic of the oil reservoir, and when an acoustic field is applied, the formation of wave processes takes place in it. The resulting acoustic emission is represented by both a discrete, pulsed, and continuous noise-like component [3] [4].

2. Nonlinearity of Caused Acoustic Emission Investigation in the Oil Well

The field of acoustic emission and reception of its signals in a wide frequency range is produced by devices located in a single borehole geophysical device that can move along the wellbore during well testing with a given equipment operation algorithm [2]. The equipment operation algorithm consists of the sequential execution of operations for recording the micro-seismic background in the well, acoustic impact on the mountain massif and re-registration of the signals of emission immediately after the impact. The energy of the induced acoustic emission, which is released in the process of acoustic impact, was determined by the method of calculating the spectral energy density similarly to the method of core research using the Intel Graph 2 program. **Figure 1** shows an example of an acoustic emission signal in the BS10 reservoir of a terrigenous type of the Tevlin-Russkinskoye field in Western Siberia during an acoustic impact. On average, the increase in the SAE signal after the acoustic impact in the reservoir saturated with oil is several tens of percent relative to the background level. At the same time, individual acoustic emission events in the form of single actions of emission sources occur randomly and have characteristic parameters of the signal pulses of a finite duration of a certain form. At the same time, the presence of discrete frequencies with a certain maximum energy value is clearly manifested. Spectral analysis of the acoustic emission signal with a duration of one second (**Figure 2**) is performed using a window Fourier transform, in a sliding window of a given length. The transformation parameters were selected in an optimal way to identify the details of the process in time, which are characteristic of this type of reservoir. The spectrogram shows the distinct discrete nature of the set of frequencies in the signal caused by acoustic emission. At the same time, there is an increase in the energy of acoustic emission at discrete frequencies by several times as compared with the micro-seismic background. In this spectrum, you can select some discrete frequencies, interconnected nonlinear relationship (**Table 1**). In a fractured carbonate reservoir, after acoustic impact,

Table 1. Discrete frequencies from the spectrum of the acoustic emission signal at a depth of 2840 meters.

N	"2840m"			
	$\omega(N)$	$\omega(\Sigma)$		$\Delta\omega$
1	1259			
2	2648			
3	4048	$\omega_1 + \omega_2$		-3.50%
4	6007			
5	6826	$\omega_2 + \omega_3$		-1.90%
6	8290	$\omega_2 + \omega_4$		4.40%
7	9506	$\omega_1 + \omega_6$		-0.45%
8	10,389	$\omega_3 + \omega_4$		3.21%
9	11,509	$\omega_3 + \omega_5$		5.52%

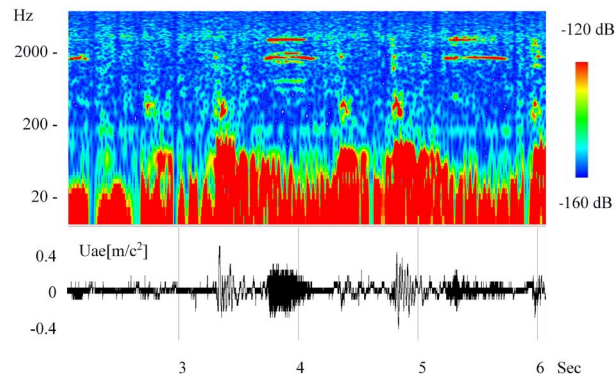


Figure 1. Acoustic emission signal and its spectrogram after acoustic impact in an oil well at a depth of 2840 meters in a terrigenous-type reservoir. U is the amplitude of acoustic response, axes X is time in sec.

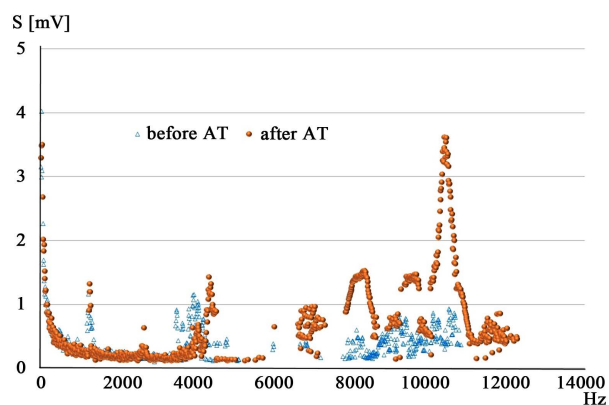


Figure 2. The spectrum of the acoustic emission signal at the point of 2840 m of the terrigenous collector before (AT, blue) and after (AT, brown) the acoustic impact. S is the spectrum amplitude.

the AE signal also has a pronounced discrete character. Moreover, after the acoustic impact, there was a significant increase in the energy of the induced acoustic emission compared with the background and the formation of pronounced discrete frequencies of energy in the spectrum of the emission signal. The nonlinearity of the radiation process caused by acoustic emission is manifested in the ratio of the main frequencies of the spectrum. But at the same time, there is a significant difference in the composition of discrete frequencies of the terrigenous and carbonate type spectra. The fractured carbonate type of collector has a much smaller number of discrete frequencies and their location in a narrower band as compared with the emission spectrum of a terrigenous collector. This is due to the different structure of the pore space of these reservoirs and the nature of changes in the dynamic processes of the stress state in them and the filtration of fluids.

In the column $\omega (N)$ it is the frequency from the spectrum in **Figure 2**, in the column $\omega (\Sigma)$ is the sum of the frequencies of the various vibration modes, and in the column $\Delta\omega$ is the difference of the frequency values measured and calculated.

The main result of this part of our research consists on that fact that the resonant frequencies of the acoustic response and their sums are in a good agreement with the measured ones: so $\omega_1 + \omega_2 = \omega_3$: $(1259 + 2648) = 3907$ and the measured frequency ω_3 is 4048, then the difference between the measured and calculated value of ω_3 is -3.5% , that value is less than the error of experimental data and that coincides with the result of connection two oscillations in a nonlinear medium [1].

3. Sound Diffraction Simulation on a Two-Dimensional Porous Oil-Saturated Reservoir of a Hierarchical Type, Located in an N-Layer Elastic Medium after Acoustic Excitation

Here we shall construct an algorithm for modeling the resonant acoustic response process of a two-phase porous hierarchical medium according to the results written in **Table 1**. We shall assume that the number N in the table will coincide with the number of the rank of hierarchical inclusions in the elastic reservoir. These inclusions will be of different features: they may have elastic features, plastic features and can be oil saturated. They can be a large inclusion, that consists of some number of fewer inclusions. And these features are linked with the sequence of 1 up to 9 of N in **Table 1**.

In the paper [5] algorithm for modeling sound diffraction on 2D elastic hierarchical inclusion located in J-th layer of the N-layered medium is written using such designations and functions.

$G_{Sp,j}(M, M^0)$ —source function of seismic field, for which the boundary problem had been formulated in the paper [6]; $k_{1ji}^2 = \omega^2(\sigma_{ji}/\lambda_{ji})$ —wave number for the longitudinal wave; the index ji denotes the identity of the properties of the medium within the heterogeneity, ja —out of heterogeneity; λ —constant Lamé; σ —density of the medium; ω —circular frequency; $\mathbf{u} = grad\varphi$ —displacement vector; φ^0 —potential of a normal seismic field in a layered medium in the absence of heterogeneity: $\varphi_{ji}^0 = \varphi_{ja}^0$. $l = 1, \dots, L$ —rank hierarchy of inclusions. Let $l = 1$. $\lambda_{ji} = \lambda_{ja} + \omega_1 \lambda_{ji(l=1)}$ [6]. $\varphi_{(l=1)-1}^0$ corresponds to the exciting field at the reservoir level. The system of equations [5] will be rewritten as (1):

$$\begin{aligned} & \frac{(k_{1ji(l=1)}^2 - k_{1j}^2)}{2\pi} \iint_{S_{C(l=1)}} \varphi_{(l=1)}(M) G_{Sp,j}(M, M^0) d\tau_M + \frac{\sigma_{ja}}{\sigma_{ji}} \varphi_{(l=1)-1}^0(M^0) \\ & - \frac{(\sigma_{ja} - \sigma_{ji(l=1)})}{\sigma_{ji(l=1)} 2\pi} \oint_{C(l=1)} G_{Sp,j} \frac{\partial \varphi_{(l=1)}}{\partial n} d\mathbf{c} = \varphi_{(l=1)}(M^0), M^0 \in S_{C(l=1)}, \\ & \frac{\sigma_{ji(l=1)}(k_{1ji(l=1)}^2 - k_{1j}^2)}{\sigma(M^0) 2\pi} \iint_{S_{C(l=1)}} \varphi_{(l=1)}(M) G_{Sp,j}(M, M^0) d\tau_M + \varphi_{(l=1)-1}^0(M^0) \\ & - \frac{(\sigma_{ja} - \sigma_{ji(l=1)})}{\sigma(M^0) 2\pi} \oint_{C(l=1)} G_{Sp,j} \frac{\partial \varphi_{(l=1)}}{\partial n} d\mathbf{c} = \varphi_{(l=1)}(M^0), M^0 \notin S_{C(l=1)} \end{aligned} \tag{1}$$

$l = l + 1$. that is: $l = 2$, inclusions $S_{C(l=2)}$ and $C_{(l=2)}$ are located inside sections $S_{C(l=1)}$ and contours $C_{(l=1)}$ correspondingly, $\lambda_{ji} = \lambda_{ji(l=1)} + \omega_2 \lambda_{ji(l=2)}$, the inclusions are plastic, ω_2 is taken from **Table 1**. $\varphi_{(l=2)-1}^0 = \varphi_{(l=1)}$. The system of Equations (1) is rewritten as:

$$\begin{aligned} & \frac{(k_{1ji(l=2)}^2 - k_{1j}^2)}{2\pi} \iint_{S_{C(l=2)}} \varphi_{(l=2)}(M) G_{Sp,j}(M, M^0) d\tau_M + \frac{\sigma_{ja}}{\sigma_{ji(l=2)}} \varphi_{(l=2)-1}^0(M^0) \\ & - \frac{(\sigma_{ja} - \sigma_{ji(l=2)})}{\sigma_{ji(l=2)} 2\pi} \oint_{C(l=2)} G_{Sp,j} \frac{\partial \varphi_{(l=2)}}{\partial n} dc = \varphi_{(l=2)}(M^0), M^0 \in S_{C(l=2)}, \\ & \frac{\sigma_{ji(l=2)}(k_{1ji(l=2)}^2 - k_{1j}^2)}{\sigma(M^0) 2\pi} \iint_{S_{C(l=2)}} \varphi_{(l=2)}(M) G_{Sp,j}(M, M^0) d\tau_M + \varphi_{(l=2)-1}^0(M^0) \\ & - \frac{(\sigma_{ja} - \sigma_{ji(l=2)})}{\sigma(M^0) 2\pi} \oint_{C(l=2)} G_{Sp,j} \frac{\partial \varphi_{(l=2)}}{\partial n} dc = \varphi_{(l=2)}(M^0), M^0 \notin S_{C(l=2)}. \end{aligned} \tag{2}$$

$l = l + 1$. that is: $l = 3$, inclusions $S_{C(l=3)m}$ and $C_{(l=3)m}$ are located inside $S_{C(l=2)}$ and $C_{(l=2)}$, $m = 1, \dots, M$ correspondingly, $\lambda_{ji} = \lambda_{ji(l=2)} + \omega_3 \lambda_{ji(l=3)}$, the inclusions are plastic also, ω_3 is taken from **Table 1**. $\varphi_{(l=3)-1}^0 = \varphi_{(l=2)}$.

The system of Equations (1) will be rewritten as [7]:

$$\begin{aligned} & \sum_1^M \left\{ \frac{(k_{1ji(l=3)m}^2 - k_{1j}^2)}{2\pi} \iint_{S_{C(l=3)m}} \varphi_{(l=3)m}(M) G_{Sp,j}(M, M^0) d\tau_M + \frac{\sigma_{ja}}{\sigma_{ji(l=3)m}} \varphi_{(l=3)-1}^0(M^0) \right. \\ & \left. - \frac{(\sigma_{ja} - \sigma_{ji(l=3)m})}{\sigma_{ji(l=3)m} 2\pi} \oint_{C(l=3)m} G_{Sp,j} \frac{\partial \varphi_{(l=3)m}}{\partial n} dc = \varphi_{(l=3)m}(M^0) + (\alpha p_2)_m \right\}, M^0 \in S_{C(l=3)m}, \\ & \frac{\sigma_{ji(l=3)}(k_{1ji(l=3)}^2 - k_{1j}^2)}{\sigma(M^0) 2\pi} \iint_{S_{C(l=3)}} \varphi_{(l=3)}(M) G_{Sp,j}(M, M^0) d\tau_M + \varphi_{(l=3)-1}^0(M^0) \\ & - \frac{(\sigma_{ja} - \sigma_{ji(l=3)})}{\sigma(M^0) 2\pi} \oint_{C(l=3)} G_{Sp,j} \frac{\partial \varphi_{(l=3)}}{\partial n} dc = \varphi_{(l=3)}(M^0), M^0 \notin S_{C(l=3)m} \quad m = 1, \dots, M. \end{aligned} \tag{3}$$

$$(\alpha p_2)_m = \left(\left(1 - \chi - \frac{K}{K_0} \right) p_2 \right)_m$$

K —compression module, χ —porosity, K_0 —true module of phase compressibility, p_2 —pore hydrostatic pressure for the m -th fluid-saturated inclusion and $\omega_3 = \omega_1 + \omega_2$; (these frequency values are taken from **Table 1**). As we can see there are some inclusions which contain the fluid. So for each inclusion the features of (αp_2) for each m are different and they are located inside the inclusions sections $S_{C(l=2)}$ and contours $C_{(l=2)}$.

$l = l + 1$, that is $l = 4$, inclusions $S_{C(l=4)}$ and $C_{(l=4)}$ are located inside sections $S_{C(l=2)}$ and contours $C_{(l=2)}$ correspondingly, $\lambda_{ji} = \lambda_{ji(l=2)} + \omega_4 \lambda_{ji(l=4)}$, ω_4 is taken from **Table 1**. $\varphi_{(l=4)-1}^0 = \varphi_{(l=2)}$. The system of equations [5] will be rewritten as:

$$\begin{aligned}
 & \frac{(k_{1ji(l=4)}^2 - k_{1j}^2)}{2\pi} \iint_{S_{C(l=4)}} \varphi_{(l=4)}(M) G_{Sp,j}(M, M^0) d\tau_M + \frac{\sigma_{ja}}{\sigma_{ji(l=4)}} \varphi_{(l=4)-1}^0(M^0) \\
 & - \frac{(\sigma_{ja} - \sigma_{ji(l=4)})}{\sigma_{ji(l=4)} 2\pi} \oint_{C(l=4)} G_{Sp,j} \frac{\partial \varphi_{(l=4)}}{\partial n} dc = \varphi_{(l=4)}(M^0), M^0 \in S_{C(l=4)}, \\
 & \frac{\sigma_{ji(l=4)}(k_{1ji(l=4)}^2 - k_{1j}^2)}{\sigma(M^0) 2\pi} \iint_{S_{C(l=4)}} \varphi_{(l=4)}(M) G_{Sp,j}(M, M^0) d\tau_M + \varphi_{(l=4)-1}^0(M^0) \\
 & - \frac{(\sigma_{ja} - \sigma_{ji(l=4)})}{\sigma(M^0) 2\pi} \oint_{C(l=4)} G_{Sp,j} \frac{\partial \varphi_{(l=4)}}{\partial n} dc = \varphi_{(l=4)}(M^0), M^0 \notin S_{C(l=4)}.
 \end{aligned} \tag{4}$$

$l = l + 1$, that is $l = 5$, inclusions $S_{C(l=5)mm}$ and $C_{(l=5)mm}$ are located inside the sections $S_{C(l=2)}$ and contours $C_{(l=2)}$, $mm = 1, \dots, MM$ correspondingly, $\lambda_{ji} = \lambda_{ji(l=4)} + \omega_5 \lambda_{ji(l=5)}$, $\varphi_{(l=5)-1}^0 = \varphi_{(l=2)}$. The system of equations [5] will be rewritten as [7]:

$$\begin{aligned}
 & \sum_1^{MM} \left\{ \frac{(k_{1ji(l=5)mm}^2 - k_{1j}^2)}{2\pi} \iint_{S_{C(l=5)mm}} \varphi_{(l=5)mm}(M) G_{Sp,j}(M, M^0) d\tau_M + \frac{\sigma_{ja}}{\sigma_{ji(l=5)mm}} \varphi_{(l=5)-1}^0(M^0) \right. \\
 & \left. - \frac{(\sigma_{ja} - \sigma_{ji(l=5)mm})}{\sigma_{ji(l=5)mm} 2\pi} \oint_{C(l=5)mm} G_{Sp,j} \frac{\partial \varphi_{(l=5)mm}}{\partial n} dc = \varphi_{(l=5)mm}(M^0) + (\alpha p_2)_{mm}, M^0 \in S_{C(l=5)mm}, \right. \\
 & \frac{\sigma_{ji(l=5)}(k_{1ji(l=5)}^2 - k_{1j}^2)}{\sigma(M^0) 2\pi} \iint_{S_{C(l=5)}} \varphi_{(l=5)}(M) G_{Sp,j}(M, M^0) d\tau_M + \varphi_{(l=5)-1}^0(M^0) \\
 & \left. - \frac{(\sigma_{ja} - \sigma_{ji(l=5)})}{\sigma(M^0) 2\pi} \oint_{C(l=5)} G_{Sp,j} \frac{\partial \varphi_{(l=5)}}{\partial n} dc = \varphi_{(l=5)}(M^0), M^0 \notin S_{C(l=5)mm} \quad mm = 1, \dots, MM. \right.
 \end{aligned} \tag{5}$$

$$(\alpha p_2)_{mm} = \left(\left(1 - \chi - \frac{K}{K_0} \right) p_2 \right)_{mm}; \quad \omega_5 = \omega_2 + \omega_3; \quad (\text{these frequency values are}$$

taken from **Table 1**).

$l = l + 1$, that is $l = 6$, inclusions $S_{C(l=6)mn}$ and $C_{(l=6)mn}$ are located inside the sections $S_{C(l=2)}$ and contours $C_{(l=2)}$, $mn = 1, \dots, MN$ correspondingly, $\lambda_{ji} = \lambda_{ji(l=2)} + \omega_6 \lambda_{ji(l=6)}$, $\varphi_{(l=6)-1}^0 = \varphi_{(l=2)}$. The system of equations [5] will be rewritten as [7]:

$$\begin{aligned}
 & \sum_1^{MN} \left\{ \frac{(k_{1ji(l=6)mn}^2 - k_{1j}^2)}{2\pi} \iint_{S_{C(l=6)mn}} \varphi_{(l=6)mn}(M) G_{Sp,j}(M, M^0) d\tau_M + \frac{\sigma_{ja}}{\sigma_{ji(l=6)mn}} \varphi_{(l=6)-1}^0(M^0) \right. \\
 & \left. - \frac{(\sigma_{ja} - \sigma_{ji(l=6)mn})}{\sigma_{ji(l=6)mn} 2\pi} \oint_{C(l=6)mn} G_{Sp,j} \frac{\partial \varphi_{(l=6)mn}}{\partial n} dc = \varphi_{(l=6)mn}(M^0) + (\alpha p_2)_{mn}, M^0 \in S_{C(l=6)mn}, \right. \\
 & \frac{\sigma_{ji(l=6)}(k_{1ji(l=6)}^2 - k_{1j}^2)}{\sigma(M^0) 2\pi} \iint_{S_{C(l=6)}} \varphi_{(l=6)}(M) G_{Sp,j}(M, M^0) d\tau_M + \varphi_{(l=6)-1}^0(M^0) \\
 & \left. - \frac{(\sigma_{ja} - \sigma_{ji(l=6)})}{\sigma(M^0) 2\pi} \oint_{C(l=6)} G_{Sp,j} \frac{\partial \varphi_{(l=6)}}{\partial n} dc = \varphi_{(l=6)}(M^0), M^0 \notin S_{C(l=6)mn} \quad mn = 1, \dots, MN. \right.
 \end{aligned} \tag{6}$$

$$(\alpha p_2)_{nm} = \left(\left(1 - \chi - \frac{K}{K_0} \right) p_2 \right)_{nm}; \quad \omega_6 = \omega_2 + \omega_4; \quad (\text{these frequency values are}$$

taken from **Table 1**).

$l = l + 1$, that is $l = 7$, inclusions $S_{C_{(l=7)nm}}$ и $C_{(l=7)nm}$ are located inside the section $S_{C_{(l=1)}}$ and contour $C_{(l=1)}$, $nm = 1, \dots, NM$ correspondingly, $\lambda_{ji} = \lambda_{ji(l=1)} + \omega_7 \lambda_{ji(l=7)}$, $\varphi_{(l=7)-1}^0 = \varphi_{(l=1)}$. The system of Equations (1) will be rewritten as [8]:

$$\sum_1^{NM} \left\{ \frac{(k_{1ji(l=7)nm}^2 - k_{1j}^2)}{2\pi} \iint_{S_{C_{(l=7)nm}}} \varphi_{(l=7)nm}(M) G_{Sp,j}(M, M^0) d\tau_M + \frac{\sigma_{ja}}{\sigma_{ji(l=7)nm}} \varphi_{(l=7)-1}^0(M^0) - \frac{(\sigma_{ja} - \sigma_{ji(l=7)nm})}{\sigma_{ji(l=7)nm} 2\pi} \oint_{C_{(l=7)nm}} G_{Sp,j} \frac{\partial \varphi_{(l=7)nm}}{\partial n} dc = \varphi_{(l=7)nm}(M^0) + (\alpha p_2)_{nm} \right\}, M^0 \in S_{C_{(l=7)nm}}, \quad (7)$$

$$\frac{\sigma_{ji(l=7)}(k_{1ji(l=7)}^2 - k_{1j}^2)}{\sigma(M^0) 2\pi} \iint_{S_{C_{(l=7)}}} \varphi_{(l=7)}(M) G_{Sp,j}(M, M^0) d\tau_M + \varphi_{(l=7)-1}^0(M^0) - \frac{(\sigma_{ja} - \sigma_{ji(l=7)})}{\sigma(M^0) 2\pi} \oint_{C_{(l=7)}} G_{Sp,j} \frac{\partial \varphi_{(l=7)}}{\partial n} dc = \varphi_{(l=7)}(M^0), M^0 \notin S_{C_{(l=7)nm}} \quad nm = 1, \dots, NM.$$

$$(\alpha p_2)_{nm} = \left(\left(1 - \chi - \frac{K}{K_0} \right) p_2 \right)_{nm}; \quad \omega_7 = \omega_1 + \omega_6; \quad (\text{these frequency values are}$$

taken from **Table 1**).

$l = l + 1$, that is $l = 8$, inclusions with sections $S_{C_{(l=8)m}}$, and contours $C_{(l=8)m}$, are located inside the section $S_{C_{(l=4)}}$ and contour $C_{(l=4)}$, $m' = 1, \dots, M'$ correspondingly, $\lambda_{ji} = \lambda_{ji(l=4)} + \omega_8 \lambda_{ji(l=8)m'}$, $\varphi_{(l=8)-1}^0 = \varphi_{(l=4)}$. The system of equations [5] will be rewritten as [7]:

$$\sum_1^{M'} \left\{ \frac{(k_{1ji(l=8)m'}^2 - k_{1j}^2)}{2\pi} \iint_{S_{C_{(l=8)m'}}} \varphi_{(l=8)m'}(M) G_{Sp,j}(M, M^0) d\tau_M + \frac{\sigma_{ja}}{\sigma_{ji(l=8)m'}} \varphi_{(l=8)-1}^0(M^0) - \frac{(\sigma_{ja} - \sigma_{ji(l=8)m'})}{\sigma_{ji(l=8)m'} 2\pi} \oint_{C_{(l=8)m'}} G_{Sp,j} \frac{\partial \varphi_{(l=8)m'}}{\partial n} dc = \varphi_{(l=8)m'}(M^0) + (\alpha p_2)_m \right\}, M^0 \in S_{C_{(l=8)m'}}, \quad (8)$$

$$\frac{\sigma_{ji(l=8)}(k_{1ji(l=8)}^2 - k_{1j}^2)}{\sigma(M^0) 2\pi} \iint_{S_{C_{(l=8)}}} \varphi_{(l=8)}(M) G_{Sp,j}(M, M^0) d\tau_M + \varphi_{(l=8)-1}^0(M^0) - \frac{(\sigma_{ja} - \sigma_{ji(l=8)})}{\sigma(M^0) 2\pi} \oint_{C_{(l=8)}} G_{Sp,j} \frac{\partial \varphi_{(l=8)}}{\partial n} dc = \varphi_{(l=8)}(M^0), M^0 \notin S_{C_{(l=8)m'}}, m' = 1, \dots, M'.$$

$$(\alpha p_2)_{m'} = \left(\left(1 - \chi - \frac{K}{K_0} \right) p_2 \right)_{m'}; \quad \omega_8 = \omega_4 + \omega_3; \quad (\text{these frequency values are}$$

taken from **Table 1**).

$l = l + 1$, that is $l = 9$, inclusions with sections $S_{C_{(l=9)mmm}}$ and contours $C_{(l=9)mmm}$ are located inside the sections $S_{C_{(l=3)}}$ and $S_{C_{(l=5)}}$ and contours $C_{(l=3)}$, and $C_{(l=5)}$ $m = 1, \dots, M$ and $mm = 1, \dots, MM$ correspondingly,

$$\sum_1^{MMM} \left\{ \frac{(k_{1ji(l=9)mm}^2 - k_{1j}^2)}{2\pi} \iint_{S_{c(l=9)mmm}} \varphi_{(l=9)mmm}(M) G_{Sp,j}(M, M^0) d\tau_M + \frac{\sigma_{ja}}{\sigma_{ji(l=9)mmm}} \varphi_{(l=9)-1}^0(M^0) - \frac{(\sigma_{ja} - \sigma_{ji(l=9)mmm})}{\sigma_{ji(l=9)mmm} 2\pi} \oint_{C(l=9)mmm} G_{Sp,j} \frac{\partial \varphi_{(l=9)mmm}}{\partial n} dc = \varphi_{(l=9)mmm}(M^0) + (\alpha p_2)_{mmm} \right\}, M^0 \in S_{C(l=5)mmm}, \tag{9}$$

$$\frac{\sigma_{ji(l=9)}(k_{1ji(l=9)}^2 - k_{1j}^2)}{\sigma(M^0) 2\pi} \iint_{S_{c(l=9)}} \varphi_{(l=9)}(M) G_{Sp,j}(M, M^0) d\tau_M + \varphi_{(l=9)-1}^0(M^0) - \frac{(\sigma_{ja} - \sigma_{ji(l=9)})}{\sigma(M^0) 2\pi} \oint_{C(l=9)} G_{Sp,j} \frac{\partial \varphi_{(l=9)}}{\partial n} dc = \varphi_{(l=9)}(M^0), M^0 \notin S_{C(l=9)mmm} \quad mmm = 1, \dots, MMM.$$

$$(\alpha p_2)_{mmm} = \left(\left(1 - \chi - \frac{K}{K_0} \right) p_2 \right)_{mmm}; \quad \omega_9 = \omega_5 + \omega_3; \text{ (these frequency values are}$$

taken from **Table 1**).

4. Conclusions

Thus, acoustic emission in porous media of reservoir rocks has the ability of permanently acting radiation. The main feature of acoustic emission is a reflection of stress relaxation and high sensitivity to external influences. In the case of fluid-filled pore space, the medium generates an induced energy of elastic energy that is adequately associated with its properties and state, and the radiation is non-linear.

Using data from **Table 1**, a variant of the system of structural adjustment algorithms for a nonlinear two-phase porous medium after its dynamic excitation is constructed. The values of the resonant frequencies are taken from the table. The rank of fluid saturated inclusions located in a porous medium with plastic properties is correlated with the number of the resonant frequencies. Such a system of algorithms was developed for the first time. That system can vary by the features (elastic, plastic and saturated) of the inclusions. By that analysis, we can take into account how many saturated inclusions can move inside the reservoir and can increase the potential oil recovery. After the first acoustic impact if it is needed, we can repeat the second impact, formulate the analogue of **Table 1** and construct the system of algorithms linked with data of a new table.

Conflicts of Interest

The authors declare no conflicts of interest regarding the publication of this paper.

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