

Comparison between Composite Column Using Limestone and Basalt Concrete

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ABSTRACT

This research is conducted to study the experimental behavior of composite steel-concrete columns with basalt additives. Various percentages of basalt are added to the concrete mixes to investigate its effect on the total axial compressive capacity of the columns. Expected failure scenarios of the columns are: concrete compressive failure, buckling of steel section, and de-bonding between steel and concrete sections. A conventional limestone composite column was used as base mix. The results of the study indicate a significant improvement in structural behavior and strength of the columns by increasing the percentage of basalt content.

Keywords: Composite Column; Basalt Mix; Jordan

1. Introduction

Composite columns using limestone were widely used from early 1900s. However, none or very little research conducted for using basalt in composite columns. Viest in his 1960 review of research, notes that the important factor in composite actions is the bond between concrete and steel [1].

The steel-concrete composite column is a new composite member that can achieve constructability and economy by filling the empty space in the steel H-flange with concrete. Composite columns are constructed with rolled or built-up steel section. The resulting members are able to support significantly higher loads than reinforced concrete columns of the same sizes.

A structural member composed of two or more dissimilar materials joined together (to act as a unit in which the resulting system) is stronger than the sum of its parts. An example in civil structures is the steel-concrete composite column in which a steel wide-flange shape (I or W shape) is filled with various percentages of basalt to be compared with base limestone concrete mix. Basalt is hard, dense volcanic igneous rock that can be found in most countries across the world.

Basaltic rocks are available in Jordan in many places especially in the Northeastern volcanic Plateau in Harrat Ash Shaam, Asi and Shalabi, 2005 [2]. Basalt is used in many countries especially in highway and airfields pavement construction (Rodsenbaum and Skene, 1995). Jor-

The basalt aggregates used in this research were tested for chemical composition at the Department of Chemistry of the University of Jordan by using the X-Ray Fluorescence (XRF) test. The results of this test are summarized in **Table 2**. Also the mechanical properties of the basalt aggregate were conducted as shown in **Table 3**. The results of three specimens for each group were averaged

dan has also a number of quarries and crushers equipped with advanced technologies and machinery to crush basaltic rocks into construction size aggregates. In conventional concrete mixes used in the construction industry in Jordan; it is customary to use limestone aggregates which are also available in great abundance. Basaltic rock aggregates are similar to limestone aggregates in many aspects [3]. **Table 1** shows the key properties of limestone and basalt aggregates in Jordan. The basalt aggregates are higher in specific gravity, and lower in absorption and abrasion loss values [3]. Based on this comparison, it is clearly obvious that basalt is likely to be more suitable than limestone for use in concrete mixes and this research will investigate this matter. In order to accomplish this objective, the researcher has devised an elaborate laboratory testing program that included conventional limestone mixes with zero%, 25%, 50%, 75% and 100% basalt. For the purpose of comparison, samples from each mix were then tested in the laboratory to determine key mix properties.

2. Experimental Program

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Table 1. Key properties of limestone and basalt aggregates used in Jordan (Courtesy of Dr. Zuhair Samarah and engineer Jamil Wrekat) [4].

Aggregate Property	(Fine) Basalt	(Coarse) Basalt	(Fine) Limestone	(Coarse) Limestone
(Apparent) Specific Gravity	2.943	2.917	2.673	2.626
SSD Specific Gravity	2.843	2.814	2.605	2.552
DRY Specific Gravity	2.791	2.765	2.558	2.508
Absorption %	1.854	1.763	2.70	3.80
Abrasion %	25.9	24.4	35.0	34.8

Table 2. Chemical composition of basaltic aggregates as determined By X-Ray fluorescence test (X.R.S) % [4].

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CO ₂	1.0				
Na ₂ O	2.97				
MgO	8.56				
$\mathrm{Al_2O_3}$	14.3				
SiO_2	45.9				
P_2O_5	0.372				
SO_3	0.0				
Cl	0.0				
$ m K_2O$	0.861				
CaO	11.1				
TiO_2	2.25				
MnO	0.174				
Fe_2O_3	1.22				
SrO	0.0				
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because their graphs are almost identical. The average deflections and strains represent one curve for each group of three specimens.

It is obvious from **Table 3** that the strength of the cubes increases gradually as the percentage of basalt increases. The dimensions of the cube were $150 \text{ mm} \times 150 \text{ mm} \times 150 \text{ mm}$.

The first author conducted laboratory tests on 18 columns. The chart in **Figure 1** shows the diagram of experimental program in this investigation. Five design mixes were used including limestone as base mix, with 25%, 50%, 75%, and 100% basalt. Three steel columns were used as reference. **Figure 1** shows percentages of basalt in the different mixes of composite columns. The cross section of all specimens was 80 mm × 160 mm, for the width and depth and their height was 1400 mm, as shown in **Figure 2**.

The geometry of the steel section was shown in **Figure** 2.

3. Laboratory Procedure

Five mixes were prepared; namely limestone (0% basalt as base mix), 25%, 50%, 75%, and 100% basalt. The composition of each mix is presented in **Table 4** [4]. The

Table 3. Compressive strength (kN) versus percentage of basalt.

Breaking Load (kN)	Percentage of Basalt	Compressive Strength (MPa)
750	0	33.4
824	25	36.6
873	50	38.8
930	75	41.33
1325	100	58.9

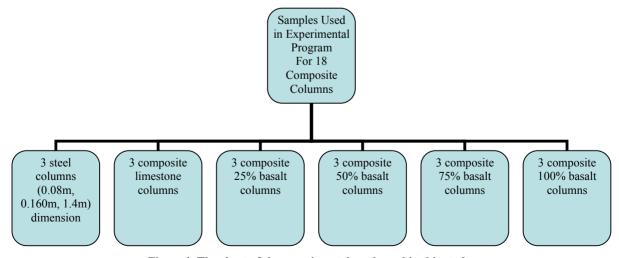


Figure 1. The chart of the experimental work used in this study.

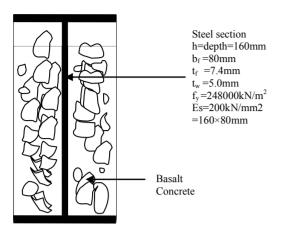


Figure 2. Typical composite cross section of the column. L = 1400 mm.

water cement ratio was 0.7 including 0.25 for hydration, and the cement was 350 kg per cubic meter of concrete.

4. Results

The center line of the composite columns were coincided with the centerline of the testing machine carefully to avoid any eccentricity and the two ends of the column were attached to the ground and to the testing machine by using rectangular steel (to avoid any horizontal movement). The mid height of the columns were marked at both sides and the dial gage (transducers) was attached to the level of marked line to measure the deflection of concentric composite columns. Similarly the other side of the column was marked, and two demic gages (transducers) (ASTM426 strain gage and BS1881:206) were attached to the column 10 cm above and below the center line. In this case the vertical distance between the two gages were 20 cm. The strain and de-flection were taken from the two gages directly by using correction factor for the testing machine for both strain and deflection. The loads were applied gradually to the specimens till failure.

There was no cyclic loading applied.

After loading the column and prior to initiation of buckling, it was noted that the specimen starts to have hair horizontal cracks (parallel to the marked line). The cracks occurred in the tension region. No cracks noticed in the compression region. The load was applied gradually to the specimen and the readings were taken at various stages of loading. For this test only ascending loading was used (no cyclic loading). Out-of-plane deformation (buckling) was measured using only one dial gage since the column is short and the width is also small. The set-up of the specimen is shown in Figures 3 and 4 with strain and deflection gages attached. The strains versus loads are shown for various percentage of basalt in Table 5 and Figure 5. As the load increases; the strain of the column increases. Each curve represents the average value for three specimens for the same load and the same percentage of basalt. The standard deviations were 0.026 and 0.076 for both deflection and strain respectively.

- 1) The three steel and limestone composite columns were taken in this experimental program as a base specimen. It was noticed that, compared with steel columns for 500 kN load, the strain and buckling decreased by 13.5% and 60%, respectively for 0% basalt. The results are shown in **Tables 5** and 6.
- 2) Now the composite columns are 25% basalt and 75% limestone, the test results show significant decrease (38% and 35%) for the strain and buckling at 600 kN load as illustrated in **Tables 5** and **6**.
- 3) In this case the three composite columns are 50% basalt and 50% limestone each, and the average results are shown in **Table 6** and in **Figure 6** for the deflection and the results were presented in **Table 5** and **Figure 5** for the strain. The strain and buckling decreased by 21.8% and 16%, respectively for the 700 kN load. Load carrying capacity increases as the percentage of basalt in composite section increases (**Table 7** and **Figure 7**).

Table 4. Percentage of basalt in composite section in the different mixes.

Sieve	%	Limestone 0% basalt	25% basalt		50% basalt		75% Basalt		100% basalt
Passing No. 4									
Sand	20	20		20	_	0	2	n	20
Basalt sand	20	20	20 20		20 20		20 20		20
(Fine)	40	20							
Passing 3/8 retained on No.4									
Medium									
	30	30	7.5 b	22.5 L	15 b	15 L	22.5 b	7.5 L	30 b
Passing 1" retained on 3/8									
Coarse									
	30	30	7.5 b	22.5 L	15 b	15 L	22.5 b	7.5 L	30 b

b = basalt, L = limestone.



Figure 3. Composite basalt column under concentric load with strain and buckling (deflection) gages (transducers).

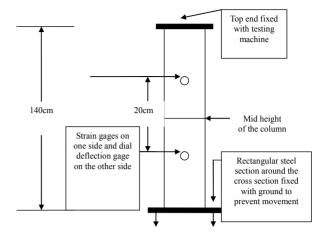


Figure 4. Location of the strain gages on one side of the column for strain.

Table 5. Load versus strain x10E-4 for various percentages of basalt.

Load (kN)	Strain (1× 10E-4) Steel	Strain (1 × 10E–4) 0% Basalt	Strain (1 × 10E–4) 25% Basalt	Strain (1 × 10E–4) 50% Basalt	Strain (1 × 10E–4) 75% Basalt	Strain (1 × 10E–4) 100% Basalt
0	0	0	0	0	0	0
200	3.9	2.64	1.7	1.5	1.44	1.20
400	7.92	6.32	4	3.76	3.68	2.16
500	11.102	9.6	5.6	5.28	5.08	2.64
600	19.76	11.76	7.2	6.8	6.48	3.36
700	-	14.96	10.24	7.8	8.0	4.24
800	-	-	24.26	10.8	10.40	5.20
900	-	-	-	-	14.00	6.24
1000	-	-	-	-	16.32	7.28
1050	-	-	-	-	-	13.44

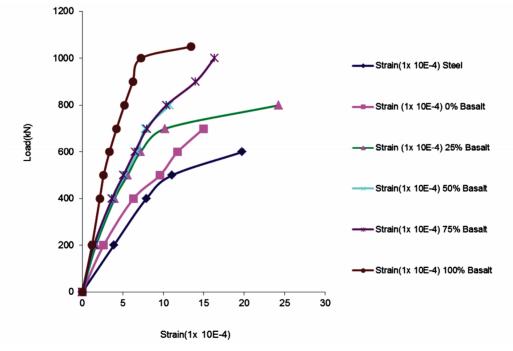


Figure 5. Load (kN) versus strain $(1 \times 10E-4)$.

Table 6. Load (kN) versus deflection (mm) for various percentages of basalt.

Load (kN)	Deflection (mm) Steel	Deflection (mm) 0% Basalt	Deflection (mm) 25% Basalt	Deflection (mm) 50% Basalt	Deflection (mm) 75% Basalt	Deflection (mm) 100% Basalt
0	0	0	0	0	0	0
200	1.45	0.63	0.38	0.29	0.26	0.12
400	2.84	0.98	0.65	0.53	0.40	0.33
500	3.48	1.39	0.94	0.80	0.60	0.49
600	5.44	1.88	1.22	1.08	0.80	0.68
700	-	3.20	2.00	1.68	1.08	0.78
800	-	-	3.44	3.38	2.65	2.28
900	-	-	-	-	6.64	5.18
1000	-	-	-	-	8.09	6.31
1050	-	=	-	-	-	7.03

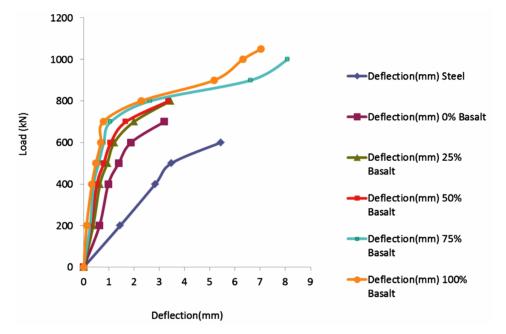


Figure 6. Load kN versus deflection (mm).

Table 7. Failure load versus percentage of basalt in composite column.

Basalt Percentage	Steel Section	(Limestone)	25%	50%	75%	100%
Failure Load (kN)	635	771	840	867	1035	1075

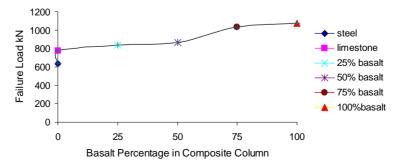


Figure 7. Failure load kN versus percentage if basalt in composite columa.

The strain gages were attached to the specimen as shown in **Figure 4**.

- 4) Three composite columns were tested with 75% basalt and 25% limestone. The average tests results for deflection are shown in **Table 6** and in **Figure 6**. The strain and buckling averages were decreased by 20.5% and 40.1% respectively. The capacity of the composite basalt columns increased by 20.6% as basalt in the mix increased from 50% to 75%.
- 5) In the case of 100% basalt composite column, deflection decreased by 22% (**Table 6** and **Figure 6**), and strain also decreased by 55.3% at load 1000 kN (**Table 5** and **Figure 5**). All the deflections results for six groups for various percentages of basalt are illustrated in **Table 6** and **Figure 6**.
- 6) The results (**Table 7** and **Figure 7**) showed significant increase in failure load as the percentage of basalt increased from 25%, 50%, 75% to 100% in composite column of about 9%, 12.5%, 34.2% and 39.4% respectively relative to the base mix (limestone). The failure load of the composite with 75% limestone and 25% basalt increased by 21% and 32% compared with steel section only.
- 7) Significant reduction in strain (54%, 65% and 71%, at 200, 400 and 700 kN respectively) took place as the composite column changed from limestone to 100% basalt as in **Table 5** and **Figure 5**.
- 8) Buckling (deflection) of the composite basalt columns decreased significantly (about 64%) compared with limestone composite columns. This reduction indicates that basalt composite columns are much stronger and more durable than those of limestone (**Table 6** and **Figure 6**).

5. Analysis of the Results

The key properties investigated in this research project included:

- 1) Lateral buckling conducted under axial concentrated load, three steel columns (0.08 m, 0.16 m, 1.4 m) and three composite columns for each mix percentage total of 15 columns.
 - 2) Strain versus load.
 - 3) Failure load for various percentages of basalt.

As the load increased gradually from 200 kN to 650 kN, the deflection at various percentages shows no significant difference, but when the load increased from 650 kN to 1050 kN, the deflection increased for the same percentage of basalt. At the same loading, the deflection decreases as the percentage of basalt increases. This indicates that the load bearing capacity of the specimens increased as the percentage of basalt increased [5] (**Table 6** and **Figure 6**). The experimental results show that the deflection of the steel column at 500 kN decrease by

60% (compared with limestone composite column), while decreased by 12%, 45%, 55%, and 69% as the percentage of basalt increased (from 25%, 50%, 75% and 100%) respectively. The strains decreased by 40.7% when comparing steel column with limestone composite column. However, as the percentage of basalt in the composite column was increased by 25%, 50%, 75% and 100%, respectively for 600 kN, the strains were correspondingly decreased by 39%, 42%, 45%, and 71%. The failure loads increased by 17.6% when comparing steel beam with composite limestone. By increasing the percentage of basalt by 25% at each stage, the failure load increased by 8.2%, 11%, 25% and 28%.

6. Acknowledgements

The author would like to thank the Tafilah Technical University for the financial support of this research project.

7. Conclusions and Recommendation for Further Research

It was noticed from the experimental work that the composite basalt column behaved better than limestone composite column. This improvement is relevant only to concentric axial compressive load conditions. Thus using composite basalt column rather than limestone column is highly recommended. To avoid any slip problems between steel and basalt concrete, the authors recommends future research on using mechanical stud connector to resist shear which may develop during bending. The stud should be attached to the web of the column to keep the bond in the composite section.

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