

# On Propagation of Rayleigh Type Surface Wave in a Micropolar Piezoelectric Medium

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## Abstract

In the present paper, the governing equations of a linear transversely isotropic micropolar piezoelectric medium are specialized for x-z plane after using symmetry relations in constitutive coefficients. These equations are solved for the general surface wave solutions in the medium. Following radiation conditions in the half-space, the particular solutions are obtained, which satisfy the appropriate boundary conditions at the stress-free surface of the half-space. A secular equation for Rayleigh type surface wave is obtained. An iteration method is applied to compute the non-dimensional wave speed of the Rayleigh surface wave for specific material parameters. The effects of piezoelectricity, non-dimensional frequency and non-dimensional material constant, charge free surface and electrically shorted surface are shown graphically on the wave speed of Rayleigh wave.

## Keywords

Piezoelectric Medium, Micro-Rotation, Transverse Isotropy, Rayleigh Wave, Wave Speed

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## 1. Introduction

The materials possessing linear coupling between mechanical and electric fields are termed as piezoelectric materials. Wave propagation in piezoelectric media has numerous applications in various fields of engineering. Some problems about propagation of plane waves in piezoelectric medium are studied by Kyame [1], Pailloux [2] and Hruska [3]. Various other problems related to the phenomena of reflection and refraction of plane waves in piezoelectric materials are studied by Auld [4], Parton and Kudryavtsev [5], Galassi, *et al.* [6], Singh [7] and Sharma [8]. Recently Salah *et al.* [9] studied the propagation of Rayleigh waves in a functionally graded piezoelectric mate-

rial half-space.

Eringen [10] [11] [12] introduced the micro-continuum field theories of solids with electro-magnetic and thermal interactions. Craciun [13] formulated the basic equations of the linear theory of piezoelectric micropolar thermoelasticity with quasi-static electric fields. Ciomasu and Vieru [14] presented the variational formulation for the free vibration of a micropolar piezoelectric body. Zhilin [15] developed a theory of the micropolar piezoelectric materials. Iesan [16] established a uniqueness result and a reciprocal theorem in the linear theory of microstretch piezoelectricity. Aouadi [17] considered the linear dynamic theory of micropolar piezoelectricity and established a reciprocity relation with two processes at different instants. Gales [18] considered the linear theory of micromorphic piezoelectricity and formulated the initial boundary value problem and presented some uniqueness results. Chen [19] derived the linear constitutive equations for micropolar electromagnetic elastic solids.

The propagation of surface waves in a transversely isotropic micropolar piezoelectric medium is not attempted so far. Following Aouadi [17], the governing equations for a transversely isotropic micropolar piezoelectric medium are formulated in x-z plane and are solved for possible surface waves. After considering the required radiation conditions in half-space and boundary conditions at free surface, a secular equation for non-dimensional wave speed of Rayleigh surface wave is obtained. The dependence of non-dimensional wave speed on frequency, material constants and electric field is shown graphically.

## 2. Governing Equations and Solution

We consider a homogeneous and transversely isotropic micropolar piezoelectric half space. We take the origin of the coordinate system on the free surface and the positive z axis along the normal into the half-space ( $z \geq 0$ ). We assume the components of the displacement and microrotation vectors of the form  $\mathbf{u} = (u_1, 0, u_3)$  and  $\boldsymbol{\varphi} = (0, \varphi_2, 0)$ . Using symmetry relations in the coefficients, the governing equations given in Aouadi [17] are specialized for x-z plane in the following from after a lengthy calculation

$$A_{11} \frac{\partial^2 u_1}{\partial x^2} + (A_{13} + A_{56}) \frac{\partial^2 u_3}{\partial x \partial z} + A_{55} \frac{\partial^2 u_1}{\partial z^2} + K_1 \frac{\partial \varphi_2}{\partial z} - (\lambda_{15} + \lambda_{31}) \frac{\partial^2 \psi}{\partial x \partial z} = \rho \frac{\partial^2 u_1}{\partial t^2} \quad (1)$$

$$A_{66} \frac{\partial^2 u_3}{\partial x^2} + (A_{13} + A_{56}) \frac{\partial^2 u_1}{\partial x \partial z} + A_{33} \frac{\partial^2 u_3}{\partial z^2} + K_2 \frac{\partial \varphi_2}{\partial x} - \lambda_{15} \frac{\partial^2 \psi}{\partial x^2} - \lambda_{33} \frac{\partial^2 \psi}{\partial z^2} = \rho \frac{\partial^2 u_3}{\partial t^2} \quad (2)$$

$$B_{77} \frac{\partial^2 \varphi_2}{\partial x^2} + B_{66} \frac{\partial^2 \varphi_2}{\partial z^2} - \chi \varphi_2 - K_1 \frac{\partial u_1}{\partial z} - K_2 \frac{\partial u_3}{\partial x} - \beta_{14} \frac{\partial^2 \psi}{\partial x^2} - \beta_{36} \frac{\partial^2 \psi}{\partial z^2} = \rho j \frac{\partial^2 \varphi_2}{\partial t^2} \quad (3)$$

$$\lambda_{15} \frac{\partial^2 u_3}{\partial x^2} + \lambda_{33} \frac{\partial^2 u_3}{\partial z^2} + (\lambda_{15} + \lambda_{31}) \frac{\partial^2 u_1}{\partial x \partial z} + \beta_{14} \frac{\partial^2 \varphi_2}{\partial x^2} + \beta_{36} \frac{\partial^2 \varphi_2}{\partial z^2} + \gamma_{11} \frac{\partial^2 \psi}{\partial x^2} + \gamma_{33} \frac{\partial^2 \psi}{\partial z^2} = 0, \quad (4)$$

where  $A_{11}, A_{13}, A_{55}, A_{56}, A_{66}, B_{66}, \lambda_{15}, \lambda_{31}, \lambda_{33}, \beta_{14}, \beta_{36}, \gamma_{11}, \gamma_{33}$  are constitutive coefficients.  $K_1 = A_{56} - A_{55}, K_2 = A_{66} - A_{56}, \chi = K_2 - K_1$ .

We seek the surface wave solution of Equations (1) to (4) in the following form

$$\{u_1, u_3, \varphi_2, \psi\} = \{\bar{u}_1(z), \bar{u}_3(z), \bar{\varphi}_2(z), \bar{\psi}(z)\} e^{ik(x-ct)} \tag{5}$$

Making use of Equation (5) in Equations (1) to (4) and applying the radiation conditions  $u_1 \rightarrow 0, u_3 \rightarrow 0, \varphi_2 \rightarrow 0, \psi \rightarrow 0$  as  $z \rightarrow \infty$ , we obtain the following particular solutions in half-space

$$u_1 = (A_1 e^{-m_1 z} + A_2 e^{-m_2 z} + A_3 e^{-m_3 z} + A_4 e^{-m_4 z}) e^{ik(x-ct)} \tag{6}$$

$$u_3 = (\zeta_1 A_1 e^{-m_1 z} + \zeta_2 A_2 e^{-m_2 z} + \zeta_3 A_3 e^{-m_3 z} + \zeta_4 A_4 e^{-m_4 z}) e^{ik(x-ct)} \tag{7}$$

$$\varphi_2 = (\eta_1 A_1 e^{-m_1 z} + \eta_2 A_2 e^{-m_2 z} + \eta_3 A_3 e^{-m_3 z} + \eta_4 A_4 e^{-m_4 z}) e^{ik(x-ct)} \tag{8}$$

$$\psi = (\xi_1 A_1 e^{-m_1 z} + \xi_2 A_2 e^{-m_2 z} + \xi_3 A_3 e^{-m_3 z} + \xi_4 A_4 e^{-m_4 z}) e^{ik(x-ct)} \tag{9}$$

where the expressions for coupling coefficients  $\xi_i, \zeta_i, \eta_i (i = 1, 2, 3, 4)$  and the relations between  $m_i (i = 1, 2, 3, 4)$  are given in *Appendix*.

### 3. Boundary Conditions

The appropriate boundary conditions at  $z = 0$  are vanishing of normal and tangential force stress components, tangential couple stress component

$$\sigma_{33} = 0, \sigma_{31} = 0, m_{32} = 0, \tag{10}$$

And vanishing of electric displacement component or electric potential

$$D_3 = 0 \text{ (for charge free case) or } \psi = 0 \text{ (for electrically shorted case),} \tag{11}$$

where

$$\sigma_{33} = A_{13}u_{1,1} + A_{33}u_{3,3} - \lambda_{35}\psi_{,1} - \lambda_{33}\psi_{,3},$$

$$\sigma_{31} = A_{56}u_{3,1} + A_{55}u_{1,3} + (A_{56} - A_{55})\varphi_2 - \lambda_{31}\psi_{,1} - \lambda_{35}\psi_{,3},$$

$$m_{32} = B_{66}\varphi_{2,3} - \beta_{36}\psi_{,3},$$

$$D_3 = \lambda_{15}u_{1,1} + \lambda_{33}u_{3,3} + \beta_{36}\varphi_{2,3} + \gamma_{33}\psi_{,3}.$$

### 4. Secular Equations

The particular solutions (6) to (9) satisfy the boundary conditions (10) and (11) at the free surface  $z = 0$  and we obtain the following secular equation

$$\begin{aligned} & A_1^* B_2^* C_3^* D_4^* - A_1^* B_2^* C_4^* D_3^* - A_1^* B_3^* C_2^* D_4^* + A_1^* B_3^* C_4^* D_2^* \\ & + A_1^* B_4^* C_2^* D_3^* - A_1^* B_4^* C_3^* D_2^* - A_2^* B_1^* C_3^* D_4^* + A_2^* B_1^* C_4^* D_3^* \\ & + A_2^* B_3^* C_1^* D_4^* - A_2^* B_3^* C_4^* D_1^* - A_2^* B_4^* C_1^* D_3^* + A_2^* B_4^* C_3^* D_1^* \\ & + A_3^* B_1^* C_2^* D_4^* - A_3^* B_1^* C_4^* D_2^* - A_3^* B_2^* C_1^* D_4^* + A_3^* B_2^* C_4^* D_1^* \\ & + A_3^* B_4^* C_1^* D_2^* - A_3^* B_4^* C_2^* D_1^* - A_4^* B_1^* C_2^* D_3^* + A_4^* B_1^* C_3^* D_2^* \\ & + A_4^* B_2^* C_1^* D_3^* - A_4^* B_2^* C_3^* D_1^* - A_4^* B_3^* C_1^* D_2^* + A_4^* B_3^* C_2^* D_1^* = 0 \end{aligned} \tag{12}$$

where

$$A_i^* = ikA_{13} - m_i \zeta_i A_{33} + m_i \xi_i \left( \lambda_{33} - \frac{ik\lambda_{35}}{m_i} \right), (i = 1, 2, 3, 4)$$

$$B_i^* = ik\zeta_i A_{56} - m_i A_{55} + (A_{56} - A_{55})\eta_i - \lambda_{31} ik\zeta_i,$$

$$C_i^* = m_i \xi_i \beta_{36} - m_i \eta_i B_{66},$$

$$D_i^* = ik\lambda_{15} - m_i \zeta_i \lambda_{33} - m_i \eta_i \beta_{36} - m_i \xi_i \gamma_{33} \quad (\text{for charge free case}),$$

Or  $D_i^* = \xi_i$  (for electrically shorted).

### 5. Particular Cases

a) The secular Equation (12) reduces for a transversely isotropic micropolar elastic case when

$$\lambda_{33} = 0, \lambda_{35} = 0, \lambda_{31} = 0, \lambda_{15} = 0, \beta_{36} = 0, \gamma_{33} = 0, \gamma_{11} = 0.$$

b) The secular Equation (12) reduces for a transversely isotropic piezoelectric case when

$$K_1 = K_2 = K = 0, A_{11} = C_{11}, A_{33} = C_{33}, A_{55} = A_{66} = A_{56} = C_{44}, A_{13} = C_{13}, B_{66} = B_{77} = 0.$$

### 6. Numerical Results and Discussion

For numerical computation of non-dimensional wave speed of Rayleigh wave, the following relevant physical constants of a transversely isotropic micropolar piezoelectric material are considered

$$A_{11} = 17.8 \times 10^{10} \text{ N} \cdot \text{m}^{-2}, \quad A_{33} = 18.43 \times 10^{10} \text{ N} \cdot \text{m}^{-2}, \quad A_{13} = 7.59 \times 10^{10} \text{ N} \cdot \text{m}^{-2},$$

$$A_{56} = 1.89 \times 10^{10} \text{ N} \cdot \text{m}^{-2}, \quad A_{55} = 4.357 \times 10^{10} \text{ N} \cdot \text{m}^{-2}, \quad A_{66} = 4.42 \times 10^{10} \text{ Nm}^{-2},$$

$$A_{65} = 1.99 \times 10^{10} \text{ N} \cdot \text{m}^{-2}, \quad B_{77} = 0.278 \times 10^9 \text{ N}, \quad B_{66} = 0.268 \times 10^9 \text{ N},$$

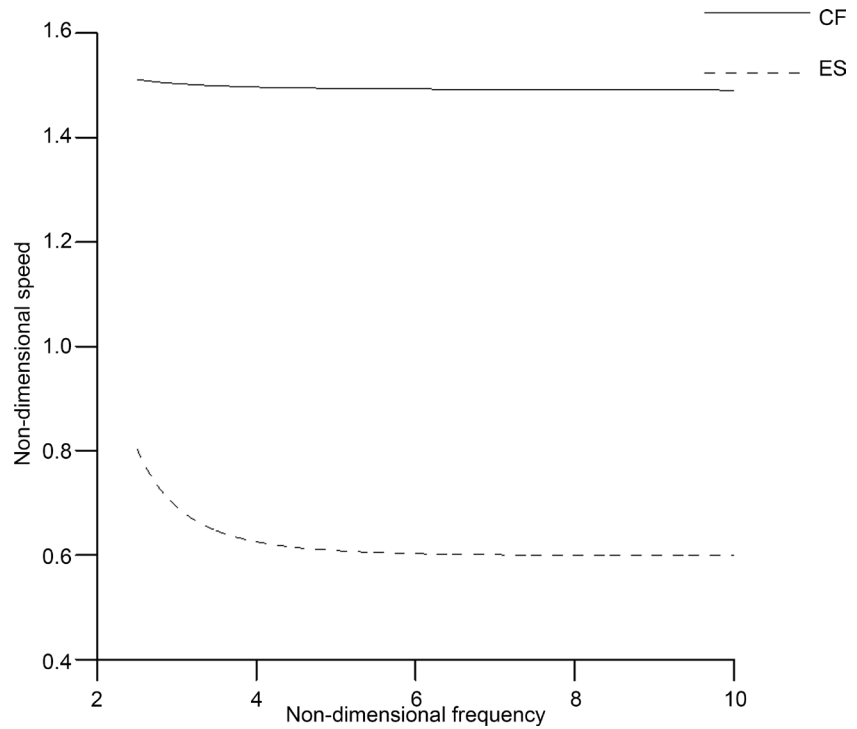
$$\lambda_{15} = 37 \text{ C} \cdot \text{m}^{-2}, \quad \lambda_{31} = 12 \text{ C} \cdot \text{m}^{-2}, \quad \lambda_{33} = 1.33 \text{ C} \cdot \text{m}^{-2}, \quad \lambda_{35} = 0.23 \text{ C} \cdot \text{m}^{-2}$$

$$\beta_{14} = 0.0001 \text{ C}, \quad \beta_{36} = 0.0002 \text{ C}, \quad \gamma_{11} = 0.000852 \text{ C}^2 \cdot \text{N}^{-1} \cdot \text{m}^{-2},$$

$$\gamma_{33} = 0.000287 \text{ C}^2 \cdot \text{N}^{-1} \cdot \text{m}^{-2}, \quad \rho = 1.74 \times 10^3 \text{ kg} \cdot \text{m}^{-3}, \quad j = 0.196 \text{ m}^2$$

For above physical constants and by using a Fortran program of Iteration method, the secular Equation (12) is solved numerically to obtain the non-dimensional speed  $\sqrt{\frac{\rho c^2}{A_{33}}}$  for certain ranges of non-dimensional frequency and non-dimensional constant.

The variation of non-dimensional speed  $\sqrt{\frac{\rho c^2}{A_{33}}}$  against non-dimensional frequency  $\left\{ \omega^* = \omega^2 / \left( \frac{\chi}{\rho j} \right) \right\}$  are shown graphically in **Figure 1** for charge free (CF) and electrically shorted (ES) cases. For CF case, the value of speed at  $\omega^* = 2.5$  is 1.5109. It decreases to a value 1.4907 at  $\omega^* = 10$ . This variation is shown by solid line in **Figure 1**. For ES case, the value of speed at  $\omega^* = 2.5$  is 0.8036. It decreases to value 0.5991 at  $\omega^* = 10$ . This variation is shown by dotted line in **Figure 1**. Comparing the solid and dotted lines in **Figure 1**, we can observe the effect of charge free surface over electrically

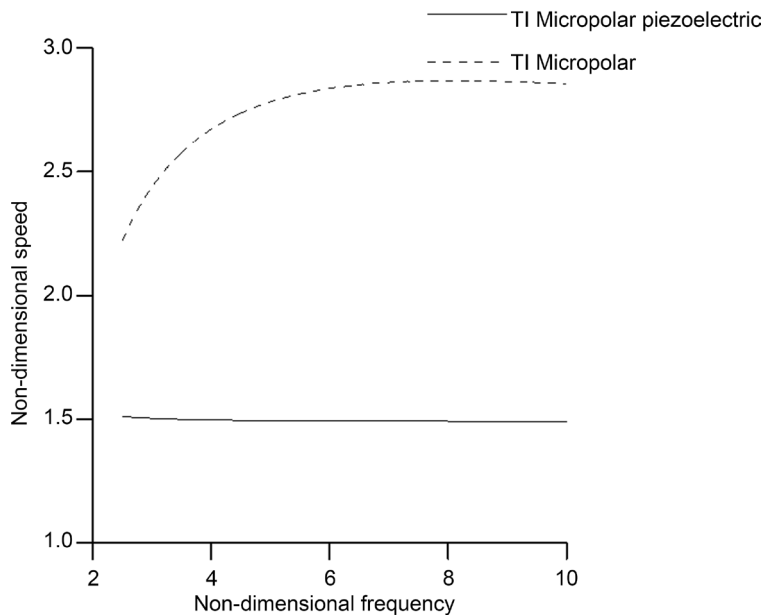


**Figure 1.** Variation of non-dimensional speed  $\sqrt{\frac{\rho c^2}{A_{33}}}$  against non-dimensional frequency  $\left\{ \omega^* = \omega^2 / \left( \frac{\chi}{\rho j} \right) \right\}$  for charge free (CF) and electrically shorted (ES) cases.

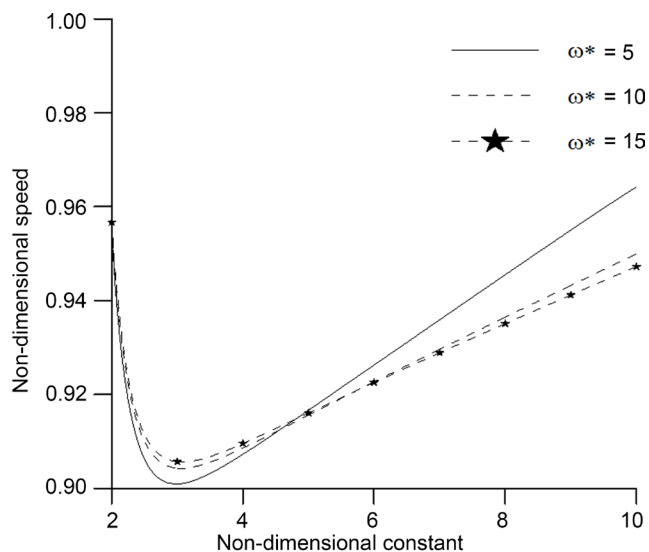
shorted surface on non-dimensional speed of the Rayleigh wave in a transversely isotropic micropolar piezoelectric solid half-space.

The variation of non-dimensional speed  $\sqrt{\frac{\rho c^2}{A_{33}}}$  is shown graphically in **Figure 2** against non-dimensional frequency  $\left\{ \omega^* = \omega^2 / \left( \frac{\chi}{\rho j} \right) \right\}$  for charge free (CF) case to observe the piezoelectric effects. The variation non-dimensional speed as shown by solid line (transversely isotropic micropolar piezoelectric case) in **Figure 2** is same as shown in **Figure 1**. For transversely isotropic micropolar case, the variation of non-dimensional speed is shown by dotted line in **Figure 2**. It has value 2.2224 at  $\omega^* = 2.5$  and it increases to value 2.8541 at  $\omega^* = 10$ . The comparison of solid and dotted lines in **Figure 2** shows the piezoelectric effect on non-dimensional speed of Rayleigh wave in a transversely isotropic micropolar piezoelectric solid half-space with charge free surface.

The variation of non-dimensional speed  $\sqrt{\frac{\rho c^2}{A_{33}}}$  is shown graphically in **Figure 3** against non-dimensional constant  $\left( \frac{A_{11}}{A_{33}} \right)$  for charge free (CF) case when  $\omega^* = 5, 10$



**Figure 2.** Piezoelectric effect on non-dimensional speed  $\sqrt{\frac{\rho c^2}{A_{33}}}$  against non-dimensional frequency  $\left\{ \omega^* = \omega^2 / \left( \frac{\chi}{\rho j} \right) \right\}$  for charge free (CF) case.



**Figure 3.** Variation of non-dimensional speed  $\sqrt{\frac{\rho c^2}{A_{33}}}$  against non-dimensional constant  $\left( \frac{A_{11}}{A_{33}} \right)$  for charge free (CF) case when  $\omega^* = 5, 10$  and 15.

and 15. For  $\omega^* = 5$ , the non-dimensional speed is 0.9541 at  $\frac{A_{11}}{A_{33}} = 2$ . It decreases to its minimum value 0.9010 at  $\frac{A_{11}}{A_{33}} = 3$  and then it increases to a maximum value 0.9642

at  $\frac{A_{11}}{A_{33}} = 10$ . For  $\omega^* = 10$ , the non-dimensional speed is 0.9559 at  $\frac{A_{11}}{A_{33}} = 2$ . It decreases to its minimum value 0.9043 at  $\frac{A_{11}}{A_{33}} = 3$  and then it increases to value 0.9499 at  $\frac{A_{11}}{A_{33}} = 10$ . For  $\omega^* = 15$ , the non-dimensional speed is 0.9567 at  $\frac{A_{11}}{A_{33}} = 2$ . It decreases to its minimum value 0.9057 at  $\frac{A_{11}}{A_{33}} = 3$  and then it increases to value 0.9472 at  $\frac{A_{11}}{A_{33}} = 10$ . The comparison of solid ( $\omega^* = 5$ ), dotted ( $\omega^* = 10$  and dotted with star ( $\omega^* = 15$ ) lines in **Figure 3** show the effect of non-dimensional frequency and non-dimensional material constant on non-dimensional speed of Rayleigh wave in a transversely isotropic micropolar piezoelectric solid half-space with charge free surface.

## 7. Conclusion

Using symmetry relations in constitutive coefficients and assuming the components of the displacement and microrotation vectors in the form  $\mathbf{u} = (u_1, 0, u_3)$  and  $\boldsymbol{\varphi} = (0, \varphi_2, 0)$ , the governing equations given in Aouadi [17] are derived as a special case for transversely isotropic micropolar piezoelectric medium in x-z plane. Rayleigh type surface wave is studied in this medium. A secular equation for non-dimensional speed of Rayleigh wave is obtained. Using Fortran program of Iteration method, the secular equation is solved numerically. The values of non-dimensional wave speed of the Rayleigh wave are obtained for a specific material modelling the medium. The non-dimensional wave speed is shown graphically against the non-dimensional frequency and the non-dimensional material constant. From theory and numerical discussion, the effects of piezoelectricity, charge free surface, electrically shorted surface, non-dimensional frequency and non-dimensional material constant are observed on non-dimensional wave speed.

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## Nomenclature

- $\mathbf{u}$  : the displacement vector.  
 $\boldsymbol{\varphi}$  : the microrotation vector.  
 $\rho$  : the mass density.  
 $j$  : the micro-inertia.  
 $\psi$  : the electrostatic potential.  
 $k$  : the wave number.  
 $c$  : the phase velocity of the wave.  
 $\omega = kc$  : the angular frequency.  
 $\sigma_{ij}$  : the force stress tensor.  
 $m_{ij}$  : the couple stress tensor.  
 $\xi_i, \zeta_i, \eta_i$  ( $i = 1, 2, 3, 4$ ) : the coupling coefficients.

## Appendix

The relations between  $m_i$ , ( $i = 1, 2, 3, 4$ ) are given as

$$m_1^2 + m_2^2 + m_3^2 + m_4^2 = S_1,$$

$$m_1^2 m_2^2 + m_2^2 m_3^2 + m_3^2 m_4^2 + m_4^2 m_1^2 = S_2,$$

$$m_1^2 m_2^2 m_3^2 + m_2^2 m_3^2 m_4^2 + m_3^2 m_4^2 m_1^2 = S_3,$$

$$m_1^2 m_2^2 m_3^2 m_4^2 = S_4,$$

$$S_1 = \left[ k^2 \left( A_{33} A_{55} \gamma_{33} P + A_{33} A_{55} B_{66} \gamma_{11} + A_{55} P \lambda_{33}^2 + A_{55} B_{66} \gamma_{33} N + A_{55} N \beta_{36}^2 + L A_{33} B_{66} \gamma_{33} + L A_{33} \beta_{36}^2 \right. \right. \\ \left. \left. + L B_{66} \lambda_{33}^2 - B_{66} \gamma_{33} M^2 - \beta_{36}^2 M^2 + A_{33} B_{66} R^2 + 2 A_{33} A_{55} \beta_{14} \beta_{36} + 2 A_{55} B_{66} \lambda_{33} \lambda_{15} - 2 M B_{66} \lambda_{33} R \right) \right. \\ \left. - K_1^2 A_{33} \gamma_{33} - K_1^2 \lambda_{33}^2 \right] / \left( A_{33} A_{55} B_{66} \gamma_{33} + A_{33} A_{55} \beta_{36}^2 + A_{55} B_{66} \lambda_{33}^2 \right),$$

$$S_2 = \left[ k^4 \left( A_{55} B_{66} \gamma_{11} N + A_{33} A_{55} \gamma_{11} P + A_{33} A_{55} \beta_{14}^2 + A_{55} \gamma_{33} N P + A_{33} \gamma_{33} L P + B_{66} \gamma_{33} L N + L N \beta_{36}^2 + A_{55} B_{66} \lambda_{15}^2 \right. \right. \\ \left. \left. + \lambda_{33}^2 L P + A_{33} B_{66} \gamma_{11} L + A_{33} P R^2 + B_{66} N R^2 - B_{66} \gamma_{11} M^2 - \gamma_{33} P M^2 + 2 A_{33} \beta_{14} \beta_{36} L + 2 A_{55} \beta_{14} \beta_{36} N \right. \right. \\ \left. \left. + 2 A_{55} \lambda_{33} \lambda_{15} P + 2 B_{66} \lambda_{33} \lambda_{15} L - 2 \beta_{14} \beta_{36} M^2 - 2 B_{66} \lambda_{15} M R - 2 \lambda_{33} M P R \right) - k^2 \left( A_{33} \gamma_{11} K_1^2 + A_{55} \gamma_{33} K_2^2 \right. \right. \\ \left. \left. + \gamma_{33} N K_1^2 + 2 \lambda_{33} \lambda_{15} K_1^2 - 2 \gamma_{33} M K_1 K_2 - 2 \lambda_{33} R K_1 K_2 \right) \right] / \left( A_{33} A_{55} B_{66} \gamma_{33} + A_{33} A_{55} \beta_{36}^2 + A_{55} B_{66} \lambda_{33}^2 \right),$$

$$S_3 = \left[ k^6 \left( A_{55} \gamma_{11} N P + A_{55} \beta_{14}^2 N + B_{66} \gamma_{11} L N + A_{33} \gamma_{11} L P + A_{33} \beta_{14}^2 L + \gamma_{33} L N P + A_{55} \lambda_{15}^2 P + B_{66} \lambda_{15}^2 L \right. \right. \\ \left. \left. - \gamma_{11} M^2 P - \beta_{14}^2 M^2 + P R^2 N + 2 \beta_{14} \beta_{36} L N + 2 \lambda_{33} \lambda_{15} L P - 2 \lambda_{15} M P R \right) - k^4 \left( A_{55} \gamma_{11} K_2^2 + \gamma_{33} L K_2^2 \right. \right. \\ \left. \left. + \gamma_{11} N K_1^2 + \lambda_{15}^2 K_1^2 + K_2^2 R^2 - 2 K_1 K_2 \gamma_{11} M - 2 K_1 K_{215} R \right) \right] / \left( A_{33} A_{55} B_{66} \gamma_{33} + A_{33} A_{55} \beta_{36}^2 + A_{55} B_{66} \lambda_{33}^2 \right)$$

$$S_4 = \left[ k^8 \left( \gamma_{11} L N P + \beta_{14}^2 L N + \lambda_{15}^2 L P \right) - k^6 \left( \gamma_{11} L K_2^2 \right) \right] / \left( A_{33} A_{55} B_{66} \gamma_{33} + A_{33} A_{55} \beta_{36}^2 + A_{55} B_{66} \lambda_{33}^2 \right)$$

$$L = (A_{11} - \rho c^2), M = (A_{13} + A_{56}), N = (A_{66} - \rho c^2),$$

$$P = \left( B_{77} - \rho j c^2 + \frac{\chi}{k^2} \right), R = (\lambda_{15} + \lambda_{31})$$

and

$$\zeta_i = \frac{[p_i q_i + (u_i - v_i r_i)]}{q_i s_i + t_i r_i}, \quad \xi_i = \frac{p_i - s_i \zeta_i}{r_i}, \quad \eta_i = \frac{\left[ w_i - \left( iM \zeta_i \frac{m_i}{k} - iR \xi_i \frac{m_i}{k} \right) \right]}{K_1 \frac{m_i}{k}}$$

$$p_i = \left( iK_2 A_{55} \frac{m_i^2}{k^2} - iK_2 L - iMK_1 \frac{m_i^2}{k^2} \right),$$

$$q_i = \left\{ \left( \beta_{36} \frac{m_i^2}{k^2} - \beta_{14} \right)^2 + \left( \gamma_{33} \frac{m_i^2}{k^2} - \gamma_{11} \right) \left( B_{66} \frac{m_i^2}{k^2} - P \right) \right\},$$

$$r_i = \left( RK_2 \frac{m_i}{k} - \lambda_{15} K_1 \frac{m_i}{k} + \lambda_{33} K_1 \frac{m_i^3}{k^3} \right),$$

$$s_i = \left( NK_1 \frac{m_i}{k} - MK_2 \frac{m_i}{k} - A_{33} K_1 \frac{m_i^3}{k^3} \right),$$

$$t_i = \left\{ -iK_2 \left( \beta_{36} \frac{m_i^2}{k^2} - \beta_{14} \right) - \left( \lambda_{33} \frac{m_i^2}{k^2} - \lambda_{15} \right) \left( B_{66} \frac{m_i^2}{k^2} - P \right) \right\},$$

$$u_i = -\frac{m_i}{k} K_1 \left( \beta_{36} \frac{m_i^2}{k^2} - \beta_{14} \right), \quad v_i = iR \frac{m_i}{k} \left( B_{66} \frac{m_i^2}{k^2} - P \right), \quad w_i = \left( A_{55} \frac{m_i^2}{k^2} - L \right).$$



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