

Ab Initio Calculations Study of Structural and Electronic Properties of Ternary Alloy $\text{Al}_x\text{In}_{1-x}\text{As}$

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Received July 17th, 2012; revised August 20th, 2012; accepted September 16th, 2012

ABSTRACT

First principles calculations of the structural and electronic properties of AIAs, InAs and their alloy $\text{Al}_x\text{In}_{1-x}\text{As}$ have been performed using the full-potential linear muffin-tin orbital (FP-LMTO) [1] method within density functional theory (DFT) [2,3]. We used the local density approximation (LDA) [4] within the generalized gradient correction (GGA) [5] to calculate the electronic structure at equilibrium volume. The effect of composition on lattice constants, bulk modulus and band gap were investigated. Deviations of the lattice constants from Vegard's law and the bulk modulus were observed for this alloy. The microscopic origins of the gap bowing were explained by using the approach of Zunger and co-workers [6-9].

Keywords: FP-LMTO; DFT; Arsenide Compounds; Band Gap Bowing; Effective Masses

1. Introduction

The III-V group compounds XAs ($X = \text{Al}, \text{Ga}$ and In) with binary octets of $\text{A}^{\text{N}}\text{B}^{8-\text{N}}$ type have drawn profound attention recently, because of their scientific applications in fabricating heterostructures and tunable devices in the visible wavelength region, optoelectronic devices, explicitly in the high frequency range, etc. [10]. The performance of the devices strongly depends on the inherent thermodynamic and transport properties of these compounds, for example, the dielectric constants and phonon frequencies. Kamioka *et al.* [11] and Lockwood *et al.* [12] determined experimentally the dielectric constants and phonon frequencies for zinc blende type XAs at normal conditions. The band structure and density of state (DOS) of XAs have been studied and discussed by theoretical investigations [13-18]. The dielectric function also has been investigated corresponding to the band gap transition for AIAs [18,19]. Moreover, a number of experimental and theoretical studies on the lattice dynamical characteristics have been carried out, including some on the vibrational properties of the XAs alloys [10-19].

The semiconductors (BAs, AIAs, GaAs and InAs) are important materials in the fields of fabrication of micro-waves, optoelectronic, and electronic devices; they provide a good basis for many established commercial and new technological applications such as light emitting

diodes, lasers, integrated circuits, modulators, photo-detectors and filters [20]. III .arsenide compounds belong to a family of common-anion III-V semiconductors.

They have the widest range of energy gaps apart from III-nitrides and under normal conditions; these materials crystallize in the zinc blende structure [21]. Aluminum arsenide (AIAs) is indirect band gap semiconductor; it's one of the most important electronic and optoelectronic materials because of its frequent incorporation into GaAs-based hetero-structures [21,22]. While Indium arsenide (InAs) is a direct band gap semiconductor, it's used for construction of infrared detectors, for the wavelength range of 1 - 3.8 μm . The detectors are usually photovoltaic photodiodes. Cryogenically cooled detectors have lower noise, but InAs detectors can be used in higher-power applications at room temperatures as well. Indium arsenide is also used for making of diode lasers. AIAs, GaAs and InAs are fundamentals to a wide variety of optoelectronic hetero-junction systems. This includes short period super-lattice $(\text{GaAs})_m/(\text{AIAs})_n$ and $(\text{InAs})_n/(\text{GaAs})_m$ [23], bulk alloys such as $\text{Al}_x\text{In}_{1-x}\text{As}$ and $\text{In}_x\text{Ga}_{1-x}\text{As}$ [24]. InAs is well known for its high electron mobility and narrow energy band gap. It's widely used as terahertz radiation source as it is a strong photo-Dember emitter [25].

Aluminum indium arsenide is a semiconductor material with very nearly the same lattice constant as GaInAs; but a larger band gap is used as a buffer layer in meta-

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morphic HEMT transistors, it can be also used to form alternate layers with GaInAs, which act as quantum wells; these structures are used in broad band quantum cascade lasers. The toxicology of AlInAs has not been fully investigated; the dust is an irritant to skin, eyes and lungs. The environment, health and safety aspects of $\text{Al}_x\text{In}_{1-x}\text{As}$ (such as trimethylindium and arsine) and industrial hygiene monitoring studies of standard MOVPE sources have been reported in a review [26].

2. Computational Details

Electronic configurations are: **Al:** $\text{Ne}3s^23p^1$; **As:** $\text{Ne}3d^{10}4s^24p^3$ and **In:** $\text{Kr}4d^{10}5s^25p^1$. Atoms in zinc blende structure are in FCC positions as X (0, 0, 0); As (1/4, 1/4, 1/4) where X (=Al, In). In order to compute equilibrium structural parameters and electronic band structure of AlAs, InAs and their ternary alloy $\text{Al}_x\text{In}_{1-x}\text{As}$, we have employed the available Lmtart code [27]. This includes full potential linearised muffin-tin orbitals (FP-LMTO) method [1] within the density functional theory (DFT) [2,3] by using the local density approach (LDA) [4] and the gradient generalized approach (GGA) [5]. The FP-LMTO method treats muffin-tin spheres (MTs) and interstitial regions (IRs) on the same footing, leading to best precision of the eigenvalues. At the same time, the FP-LMTO method, in which the space is divided into an IR and non-overlapping (MT) spheres surrounding the atomic sites, uses a more complete basis than its predecessors. In the IR regions, the basic functions are repre-

sented by Fourier series. Inside the MT spheres, the basic functions are expanded in combinations of spherical harmonics functions. A short description of this method can be found in Ref. [28]. The values of the sphere radii (MTs) and the number of plane waves (NPLW) used in our calculations are listed in **Table 1**.

We have made an application on unit cells containing eight atoms in order to stimulate $x = 0.25$; 0.50 and 0.75 by substituting In atoms by Al atoms in the cation sublattice of ZB phases.

3. Results and Discussion

3.1. Structural Properties

To test the reliability of the *ab initio* method and the simulated results, determinations of the lattice parameters of binary compounds AlAs and InAs have been done by minimization of the total energy, than a best fitting by using the Murnaghan equation of state [29]. Our results are given in the **Table 2** (in a.u.) and there are in well agreement with those obtained experimentally. We note that the LDA underestimated the lattice parameters and overestimated the bulk modulus while the GGA overestimated the lattice parameters.

The lattice parameters (a) of ternary alloy can be expressed as a linear combination of the lattice constants of the two forming binary alloys, the physical properties of ternary alloy are usually investigated based on Vegard's law [30,31]:

Table 1. The plane wave number PW, energy cutoff (in Ry) and muffin-tin radius (RMT) (in a.u) used in calculation for binary InAs, AlAs and their ternary $\text{Al}_x\text{In}_{1-x}\text{As}$ alloy in zinc-blende (ZB) structure.

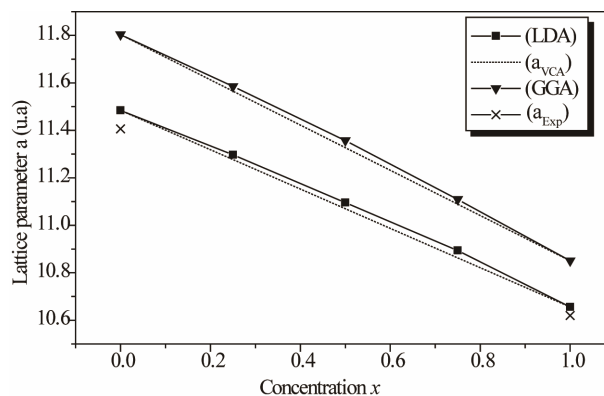
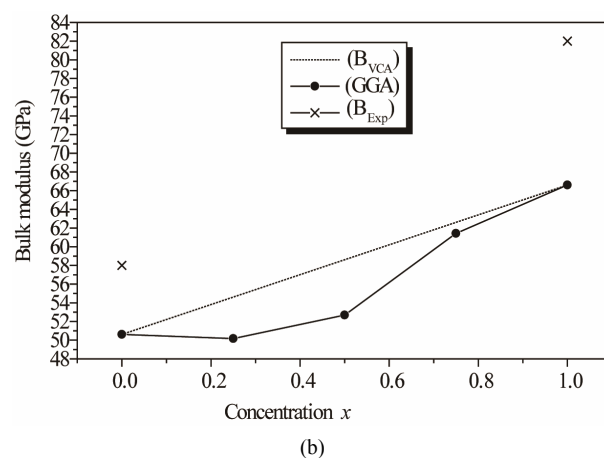
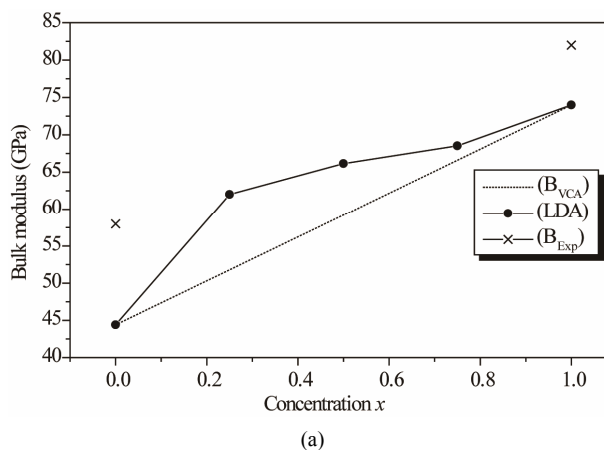
x	PW		E _{cut} . total (Ry.)			RMT (a.u)	
	LDA	GGA	LDA	GGA		LDA	GGA
0	5064	12050	86.20589	145.3981	In	2.486	2.552
					As	2.486	2.552
0.25	33421	67265	130.354	198.674	Al	2.494	2.558
					In	2.494	2.458
					As	2.396	2.558
0.50	33421	67265	135.702	208.423	Al	2.402	2.507
					In	2.402	2.507
					As	2.402	2.409
0.75	33421	67265	145.926	231.231	Al	2.401	2.405
					In	2.401	2.405
					As	2.401	2.405
1	5064	12050	100.1225	171.6997	Al	2.261	2.302
					As	2.353	2.396

Table 2. The structural properties (lattice parameter a , bulk modulus B and its pressure derivative B' for AlAs, InAs and their ternary alloy.

Compounds	a_{eq} (Å)	B_0 (GPa)	B'_0
InAs			
Present	6.077 ^{LDA}	51.21 ^{LDA}	5.122 ^{LDA}
	6.239 ^{GGA}	50.62 ^{GGA}	2.830 ^{GGA}
Exp.	6.036 [34]	58.00 [35]	4.790 [36]
Others	5.921 [37]	61.70 [37]	4.545 [37]
	6.036 [38]	60.00 [38]	
	5.902 [39]	61.90 [39]	
	6.030 [40]	60.90 [40]	4.691 [40]
	6.195 [40]	48.10 [40]	4.683 [40]
AlAs			
Present	5.639 ^{LDA}	74.296 ^{LDA}	
	5.742 ^{GGA}	66.008 ^{GGA}	
Exp.	5.620 [34]	82.00 [35]	4.182 [35]
Others	5.633 [40]	75.10 [40]	4.512 [40]
	5.734 [40]	66.50 [40]	4.184 [40]
	5.644 [41]	75.40 [41]	4.400 [41]
$\text{Al}_{0.25}\text{In}_{0.75}\text{As}$	5.978 ^{LDA}	62.012 ^{LDA}	5.753 ^{LDA}
	6.131 ^{GGA}	50.17 ^{GGA}	4.22 ^{GGA}
$\text{Al}_{0.50}\text{In}_{0.50}\text{As}$	5.871 ^{LDA}	66.156 ^{LDA}	4.899 ^{LDA}
	6.009 ^{GGA}	52.69 ^{GGA}	4.72 ^{GGA}
$\text{Al}_{0.75}\text{In}_{0.25}\text{As}$	5.765 ^{LDA}	68.524 ^{LDA}	4.04 ^{LDA}
	5.878 ^{GGA}	61.42 ^{GGA}	4.05 ^{GGA}

$$a_{\text{Al}_x\text{In}_{1-x}\text{As}} = x \cdot a_{\text{AlAs}} + (1-x) \cdot a_{\text{InAs}} \quad (1)$$

where, a_{AlAs} , a_{InAs} and $a_{\text{Al}_x\text{In}_{1-x}\text{As}}$ are, respectively, the lattice constant of the compounds AlAs, InAs and $\text{Al}_x\text{In}_{1-x}\text{As}$. In **Figures 1** and **2**, we present a comparison between results obtained for the calculated lattice parameters and the bulk modulus and those obtained from Vegard's law, that correspond to the zinc blende configuration of the ternary alloy $\text{Al}_x\text{In}_{1-x}\text{As}$ at different concentration x . In **Figure 1** we show that the lattice constant (a) of the ternary alloy decreases with an increase in Al concentration, in the both approximations LDA and GGA. The lattice parameters scale linearly with concentration thus obeying Vegard's law [30,31]. Our results show a marginal upward bowing parameters equal to -0.06057 \AA and 1.06171 \AA with both approximations LDA and GGA respectively. It's clear that this phenomenon occurs because the atom of Aluminum (Al)

**Figure 1. Composition dependence of the calculated lattice parameters within GGA (down triangle) and LDA (solid square) of $\text{Al}_x\text{In}_{1-x}\text{As}$ alloy compared with Vegard's prediction (dot line).****Figure 2. Composition dependence of the calculated bulk modulus within LDA (Solid square) (a) and GGA (Up Triangle) (b) of $\text{Al}_x\text{In}_{1-x}\text{As}$ alloy compared with Vegard's prediction.**

is smaller than that of Indium (In). Hence, the lattice parameter can be written as

$$a_{\text{Al}_x\text{In}_{1-x}\text{As}} = x \cdot a_{\text{AlAs}} + (1-x) \cdot a_{\text{InAs}} - x \cdot (1-x) b \quad (2)$$

where the quadratic term b is the bowing parameter. In **Figures 2(a)** and **(b)**, we observe that the bulk modulus increases with Al concentration. A large deviation of the bulk modulus from the linear concentration dependence (LCD) with an upward bowing parameter equal to -13.52686 GPa by using the LDA approximation; while the GGA approximation gave downward value of 18.61257 GPa. The deviation from LCD should be mainly due to the bulk modulus mismatch between AlAs and InAs compounds. A more precise comparison for the behavior of the Al_xIn_{1-x}As ternary alloy shows that a decrease of the lattice constant is accompanied by an increase of the bulk modulus. It represents bond strengthening or weakening effect induced by changing the concentration.

3.2. Electronic Properties

The calculated band structure energies of binary compounds as well as their alloy by using the FP-LMTO method within both the local density approximation (LDA) and the generalized gradient correction (GGA) exhibit an indirect gap at X point for AlAs and a direct gap at Γ point for InAs. There is an indirect gap at R point in the ternary alloy with GGA for which the band gap energy in **Figure 3**.

The band gap energy of Al_xIn_{1-x}As can be depicted as a function of the aluminum composition x , and be expressed by using the following formula:

$$E_g(x) = x \cdot E_{(AlAs)} + (1-x) \cdot E_{(InAs)} - x \cdot (1-x)b \quad (3)$$

where $E_g(x)$ denotes the band gap energy of Al_xIn_{1-x}As, and $E_{g(AlAs)}$ and $E_{g(InAs)}$ denote the band gap energy of AlAs and InAs, respectively, and b is the band gap bowing parameter of Al_xIn_{1-x}As.

Our results are given in **Table 3**. It is well known that the GGA and LDA usually underestimated the energy gap [32]. We note that a calculation of the band gap for our basic semiconductor InAs gives the result $E_g = 0.00$ eV which seems to be smaller than the literature values, and the same for the AlAs semiconductor, this is due to the well-known and systematical underestimation of DFT in GGA and LDA approaches. Note that this band gap underestimation doesn't affect the conclusions made.

$$b_{VD} = \frac{E_{AlAs}(a_{AlAs}) - E_{AlAs}(a)}{1-x} + \frac{E_{InAs}(a_{InAs}) - E_{InAs}(a)}{x} \quad (4)$$

$$b_{CE} = \frac{E_{AlAs}(a)}{1-x} + \frac{E_{InAs}(a)}{x} - \frac{E_{AllInAs}(a)}{x(1-x)} \quad (5)$$

$$b_{SR} = \frac{E_{AllInAs}(a) - E_{AllInAs}(a_{eq})}{x(1-x)} \quad (6)$$

In order to derive a phenomenological model for

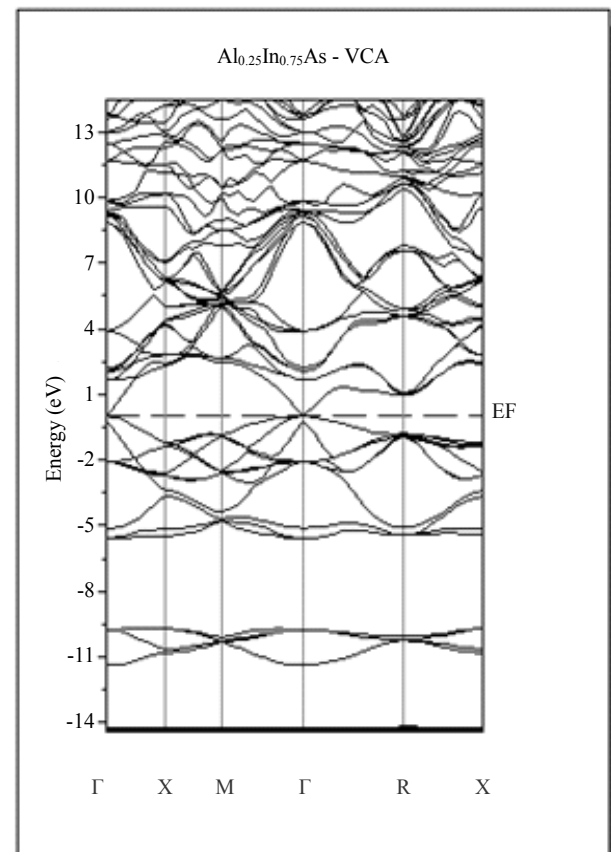
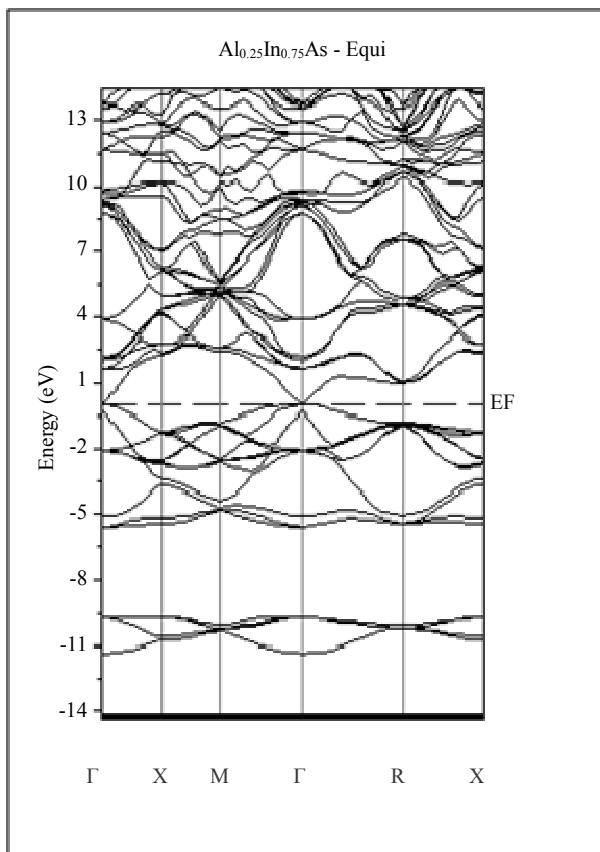
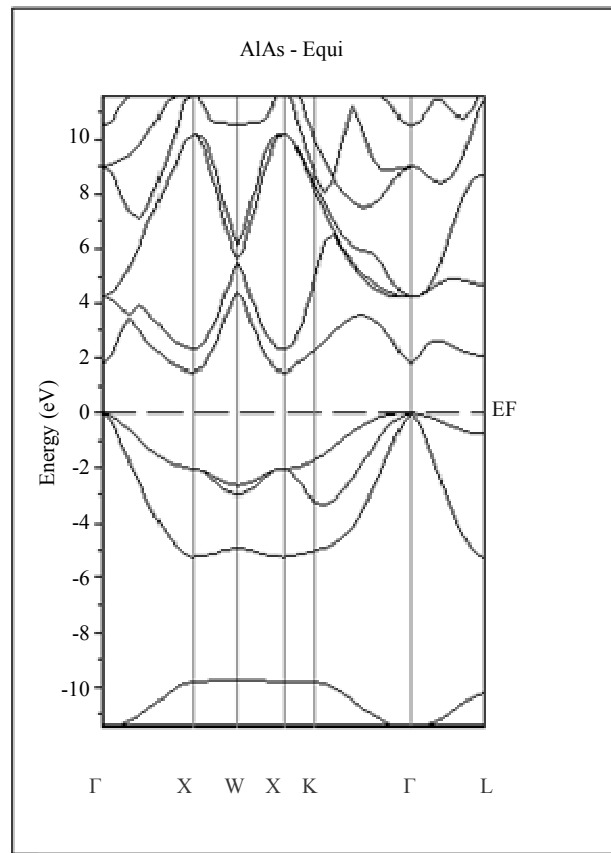
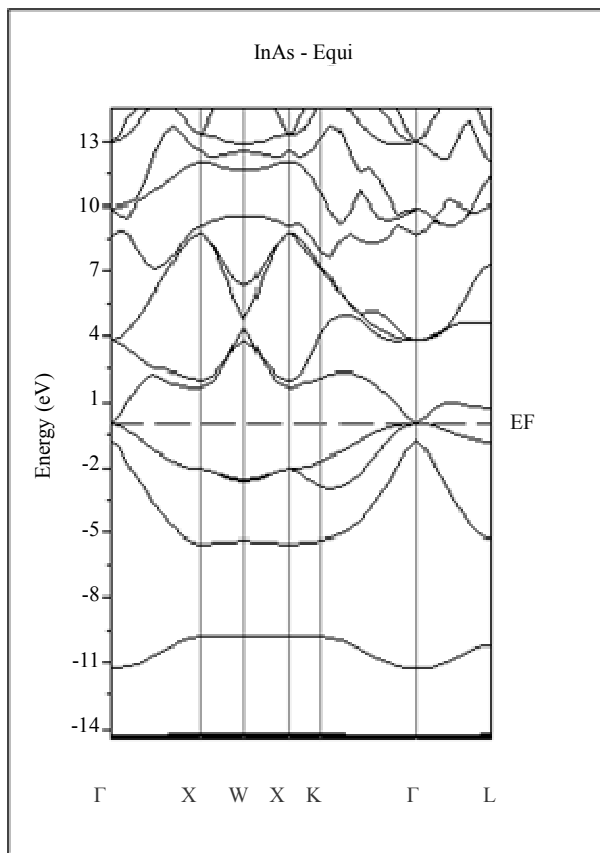
computing the band gap bowing (b), we decompose b into three physically distinct contributions [33]; 1) volume deformation (VD); 2) charge exchange (CE); and 3) structural relaxation (SR). The (VD) term represented the relative response of the binary compounds (AlAs) and (InAs) to the hydrostatic pressure from their individual equilibrium lattice constant to the alloy value $a(x)$. The second contribution, the charge exchange (CE) is related to a charge transfer in bringing (AlAs) and (InAs) at $a = a(x)$. Finally, the (SR) term described the change in the band gap upon passing from the unrelaxed to the relaxed alloy, *i.e.*, $a(x) \rightarrow a_{(eq)}$ by construction the total bowing (b) which is given in Equation (7):

$$b = b_{VD} + b_{CE} + b_{SR} \quad (7)$$

The calculated total optical band gap bowing (b) and its three contributions (b_{VD} , b_{CE} and b_{SR}) are given in **Table 4**, we note that from $x = 0.25$ to 0.75 , the main contribution to the gap bowing raises from the VD effect, whereas, for $x = 0.75$, the contribution of SR is increase. **Figure 4** shows the variation of the band gap bowing versus concentration. The bowing remains linear and varies slowly for $x = 0.50$, it decreases faster which checked the evaluation of the parameters of constants and the gap according to concentration: the calculated gap bowing parameter coefficient b for the ternary alloy ranges from 1.97 eV ($x = 0.25$) to 0.73 eV ($x = 0.75$) for the GGA and from 1.81 eV ($x = 0.25$) to 0.59 eV ($x = 0.75$) for the LDA.

3.3. Effective Masses

An effective mass is an important material parameter describing most of carrier transport properties in semiconductors [49,50]. Its importance becomes recently even greater as the technology of optoelectronic devices matures and its precise knowledge becomes critical. Its values, however, known from scientific literature for a given semiconductor material, differ usually considerably from one another. The knowledge of effective masses of electrons and holes is important for the excitonic properties of the investigated compounds. Experimentally, the effective masses are usually determined by cyclotron resonance, electro reflectance measurements or from analysis of transport data or transport measurements [51]. Theoretically, the effective masses can be estimated from the energy band curvatures. Generally, the effective mass is a tensor with nine components, however for the much idealized simple case, where the $E(k)$ diagram can be fitted by a parabola $E = \hbar^2 k^2 / 2m^*$, the effective mass becomes a scalar at high symmetry point in the Brillouin zone. Therefore, we have calculated the effective mass of electrons and holes using GGA scheme. We have computed the electron effective mass at the conduction



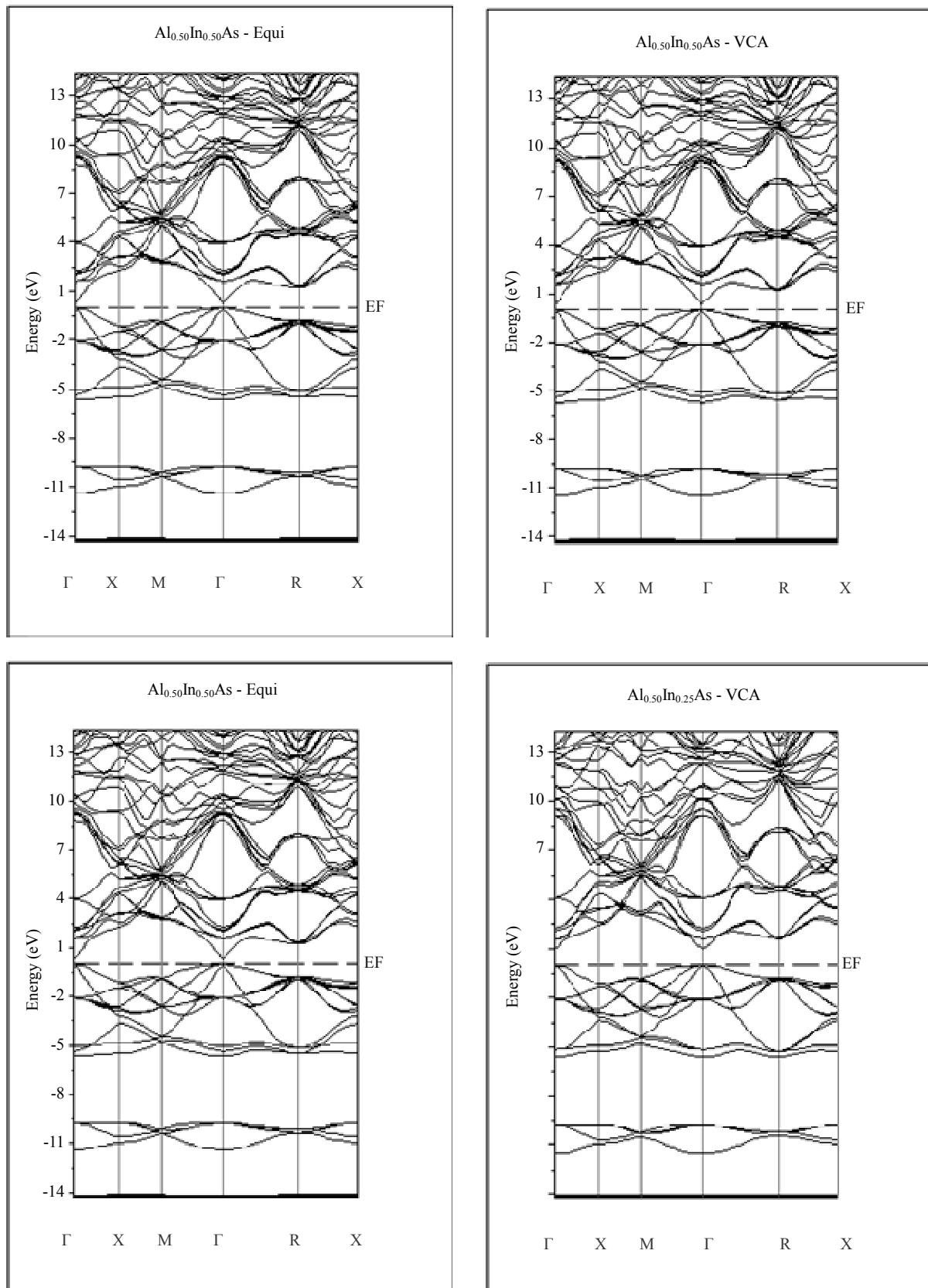


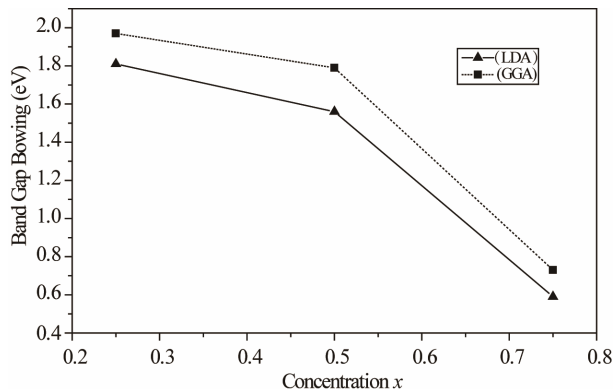
Figure 3. Band structures of zinc blende for AlAs, InAs and $Al_xIn_{1-x}As$ along the principle high symmetry directions in the Brillouin zone with GGA.

Table 3. The energy band gap (E_g) of AlAs, InAs and their ternary alloy $\text{Al}_x\text{In}_{1-x}\text{As}$.

Concentration x	Method	XC	E_g (eV)	Type of band gap	
0	Present	FP-LMTO	LDA	0.000	direct ($\Gamma - \Gamma$)
		GGA	0.000	direct ($\Gamma - \Gamma$)	
		GGA	1.680	Indirect ($\Gamma - X$)	
	Exp.		0.420 [20]	direct ($\Gamma - \Gamma$)	
	Others	FP-LAPW	LDA	0.000 [40]	direct ($\Gamma - \Gamma$)
			GGA	0.000 [40]	direct ($\Gamma - \Gamma$)
		GGA-EV	0.400 [40]	direct ($\Gamma - \Gamma$)	
		FP-LAPW	LDA	-0.64 [42]	direct ($\Gamma - \Gamma$)
		PP-PW	LDA	0.000 [43]	direct ($\Gamma - \Gamma$)
	0.25	Present	FP-LMTO	LDA	0.000
GGA			0.939	Indirect ($\Gamma - R$)	
GGA			0.000	direct ($\Gamma - \Gamma$)	
0.50	Present	LDA	0.000	direct ($\Gamma - \Gamma$)	
		GGA	1.200	Indirect ($\Gamma - R$)	
		GGA	0.290	direct ($\Gamma - \Gamma$)	
0.75	Present	LDA	0.611	direct ($\Gamma - \Gamma$)	
		GGA	1.540	Indirect ($\Gamma - R$)	
		GGA	0.970	direct ($\Gamma - \Gamma$)	
1	Present	LDA	1.360	Indirect ($\Gamma - X$)	
		GGA	1.480	Indirect ($\Gamma - X$)	
		GGA	1.740	direct ($\Gamma - \Gamma$)	
	Exp.		2.240 [20]	Indirect ($\Gamma - X$)	
	Others	FP-LAPW	LDA	1.310 [40]	Indirect ($\Gamma - X$)
			GGA	1.400 [40]	Indirect ($\Gamma - X$)
		GGA-EV	2.250 [40]	Indirect ($\Gamma - X$)	
		PP-PW	GGA	1.390 [44]	Indirect ($\Gamma - X$)
		PP-PW	LDA	1.350 [44]	Indirect ($\Gamma - X$)
	FP-LAPW	LDA	1.370 [45]	Indirect ($\Gamma - X$)	

Table 4. Decomposition of optical bowing into volume deformation (VD), charge exchange (CE) and structural relaxation (SR) contributions for $\text{Al}_x\text{In}_{1-x}\text{As}$ alloy (in eV).

Composition x	0.25	0.50	0.75
b_{VD}	0.85 ^{LDA}	0.41 ^{LDA}	-1.20 ^{LDA}
	1.49 ^{GGA}	1.40 ^{GGA}	0.70 ^{GGA}
b_{CE}	0.96 ^{LDA}	0.99 ^{LDA}	1.52 ^{LDA}
	0.48 ^{GGA}	0.20 ^{GGA}	-0.17 ^{GGA}
b_{SR}	0.00 ^{LDA}	0.16 ^{LDA}	0.27 ^{LDA}
	0.00 ^{GGA}	0.19 ^{GGA}	0.20 ^{GGA}
B	1.81 ^{LDA}	1.56 ^{LDA}	0.59 ^{LDA}
	1.97 ^{GGA}	1.79 ^{GGA}	0.73 ^{GGA}

**Figure 4. The calculated band gap bowing parameter in LDA (up triangle) and GGA (solid square) as a function of concentration x .**

band minima (CBM) and the hole effective mass at the valence band maxima (VBM) for the composition ranging from 0 to 1 for Al_xIn_{1-x}As. We have computed the electron effective mass at the conduction band minima (CBM) and the hole effective mass at the valence band maxima (VBM) for the composition ranging from 0 to 1 for Al_xIn_{1-x}As alloys. The electron effective mass value is obtained from the curvature of the conduction band near the X-point for AlAs and near the Γ -point at the CBM from X = 0 to 0.75. The hole effective mass value is calculated from the curvature near the Γ -point at the VBM for all concentration. From **Table 5**, it is worth mentioning that the hole (heavy and light) effective masses are strongly varied from composition to another. This could be attributed to the change of the position of the conduction band minimum (CBM). **Table 5**, gives our present values of effective masses (electron, heavy hole and light hole) for the ternary alloy Al_xIn_{1-x}As at the Γ point of the Brillouin zone at various compositions, except for x = 1, where we calculated effective masses at X point of the Brillouin zone. Our results concerning the electrons and holes are displayed in **Figure 5**. Our calculated effective masses for AlAs and InAs are found comparable to those others theoretical values. To the best of our knowledge, there are no earlier data on the effective masses of the studied alloy at 0.25, 0.5 and 0.75; we feel that our calculations can be used to cover the lack of data in the literature for this alloy.

4. Conclusion

In summary, we have performed *ab initio* calculations

Table 5. Electron (m_e^*), light hole (m_{lh}^*) and heavy hole (m_{hh}^*) effective masses (in units of free electron mass m_0) of the ternary alloy Al_xIn_{1-x}As using LDA and GGA.

Composition x		m_e^*	m_{lh}^*	m_{hh}^*
0	Present	0.035	0.454	3.942
	Others	0.040 [46]		
		0.036 [47]		
	Exp.	0.023 [48]		
0.25		0.012	0.825	2.694
0.50		0.006	0.727	2.505
0.75		0.004	0.858	3.154
1	Present	0.082	0.446	5.747
	Others	0.087 [46]		
		0.074 [46]		
		0.131 [47]		

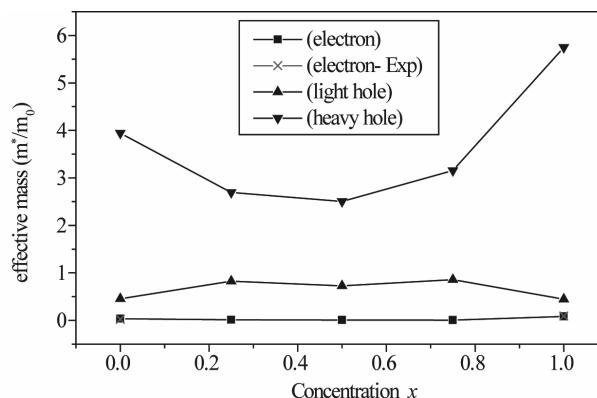


Figure 5. The effective mass (in units of free electron mass m_0) of Al composition for electron (solid square) heavy hole (down triangle) and light hole (up triangle).

using the full-potential linearised muffin-tin orbitals (FP-LMTO) method in conjunction with both the LDA and GGA approximations for exchange-correlation potential to investigate the structural and electronic properties of the zinc blende Al_xIn_{1-x}As alloy. We have calculated the concentration dependence of the lattice parameter, the bulk modulus, the band gap, bowing gap and effective masses. A linearity following the Vegard’s law with lattice parameter has been shown, but we showed a large deviation from Vegard’s law with bulk modulus. In addition, we have computed the effective masses of electron and holes. Our results provide an estimate of this important compound.

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