

# Experimental Adsorption and Modelisation of CO<sub>2</sub> on Adsorbents Collected from Elborma Field in South Tunisia

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## Abstract

In order to select the best adsorbant for CO<sub>2</sub> sequestration, this study deals the interaction between clay, Triassic sandstone and Jurassic evaporate and CO<sub>2</sub>. These materials have been used as sorbents. To choose the adequate geological layers for sequestration and with minimum risk of leakage, adsorbent characterizations were investigated using X-ray diffraction, SEM and surface area analysis, structural and textural shapes of these materials have been investigated too. The elution chromatography in gaseous phase has been employed to determine the adsorption isotherms of adsorbed CO<sub>2</sub> for each adsorbent. Then, the treatment of the experimental data allowed us to compare each CO<sub>2</sub>/adsorbent couple. The adsorption isotherms were modeled using the Langmir and Freundlich models. A thermodynamic comparison between the different adsorbents will also be provided. Experimental results show that clay and Triassic sandstone have the highest rate of adsorption amount. It has been also found that the Langmuir model is the most appropriate one to describe the phenomenon of CO<sub>2</sub> adsorption on clay. However, for the other adsorbents (*i.e.* Triassic sandstone and Jurassic evaporates) the two-models are adequate.

## Keywords

Adsorption Selectivity, Geologic Materials, Surface Area Analysis, Elution Chromatography, Langmuir, Freundlich Modelisation

## 1. Introduction

Regulating CO<sub>2</sub> emissions into the atmosphere has become a crucial target since the scientists' statement that the earth's climate is changing and the average temperature of the planet is getting higher and higher due to modern human activities [1]. In fact, greenhouse gases' concentrations are higher nowadays than that at any time previously.

To tackle this problem, geological sequestration of CO<sub>2</sub> is one of the main options to reduce CO<sub>2</sub> emissions in order to mitigate the greenhouse effect [1] [2]. Aquifers that are deep and separated from underground sources of potable water can be excellent sites for large-scale CO<sub>2</sub> storage. Moreover, a large number of such saline aquifers exist in the depths of sedimentary basins throughout the world and various solid materials such as calcium oxide or lithium oxide [3] [4] and silica gel readily adsorb carbon dioxide.

The capture and sequestration of CO<sub>2</sub> problems, actually well-documented, are classified within the scope of the general problem of the greenhouse effect and global warming particularly, through the activities of the IPCC synthesis (International Panel on Climate Change) established in 1988 under the auspices of the United Nations [5]. The CO<sub>2</sub> capture and sequestration in deep saline aquifers has emerged as an appropriate solution to reduce greenhouse gas emissions. The effectiveness of this option depends mainly on the sequestration at a low transfer rate of aquifers, sequestration potential as a residual, by adsorption or mineralization in the form of carbonate structure [6].

CO<sub>2</sub> adsorption on dry sorbents has fascinated many researchers. CO<sub>2</sub> adsorption capacity is needed for practical applications [7]. In this study, clays, Triassic sandstone and Jurassic evaporate are chosen as potential adsorbents to measure the CO<sub>2</sub> adsorption amount. These materials come from real sites considered for CO<sub>2</sub> sequestration in the southern region of Tunisia. CO<sub>2</sub> adsorption by porous materials in deep saline aquifers is a very promising option since this operation reduces the possibility of leakage from the storage tank. On the other hand, a big amount of the injected CO<sub>2</sub> in the deep aquifer can migrate to the top of the aquifer by buoyancy forces due to density difference. As a result, this quantity of CO<sub>2</sub> will be adsorbed by the cap-rock layer of the tank. This operation depends strongly on the time and physical properties of materials which comprise the cap-rock (porosity, specific surface, mineralogical composition...) and the chemical properties (acidity) as well as the nature of the adsorbed molecules.

Depending on the nature of the interactions between the adsorbent and the adsorbate, one can distinguish two-adsorption types. The first one is the physical adsorption which is attributed to lower links of physical interaction energies basically between 5 and 40 kJ/mol. The involved forces are of the Van Der Waals type due to electrostatic interactions which are small forces that can be easily broken. This is a reversible and exothermic phenomenon that can occur without changing the molecular structure of the solid [8]. However, the second one is chemical adsorption or chemisorptions, corresponding to strong chemical links with the binding energy which is large enough than 80 kJ/mol [9]. It involves chemical reactions between the surface of the adsorbent and the adsorbate molecules. It involves chemical reactions between the surface of the adsorbent and the adsorbate molecules. In this context, we are interested in assessing the best adsorbent for CO<sub>2</sub> capture. The present work aims to select an efficient adsorbent well suited to the capture of CO<sub>2</sub> and therefore to its storage for a long period of time. A study of the major intrinsic characteristics of different adsorbents will be performed. This study allowed us to evaluate the best material able to adsorb the maximum of CO<sub>2</sub> and therefore to optimize the choice of the storage site.

## 2. Materials and Methods

Three samples have been selected in this study: clay from the cap-rock layer having a green color (from the city of Gabes, Tunisia); Triassic sandstone sample which is composed of coarse sandstone and conglomerate of large siliceous stone. It is a natural adsorbent gray in color from El Borma field located in southern Tunisia, and used essentially for storage. The Jurassic evaporates are gray natural materials from deep saline aquifers in southern Tunisia, collected from the cap-rock of the reservoir. The lower layer of Jurassic evaporates is supported by a slightly discordant stratification on the Triassic sandstone.

The method used to determine the CO<sub>2</sub> adsorption isotherms on different adsorbents is based on the principle of gas-phase chromatographic method (Figure 1). Preliminary work consists in characterizing the different selected adsorbents (*i.e.* Clay, Jurassic evaporates and Triassic sandstone).

For each selected adsorbent, we are interested in determining the equilibrium conditions in the column. Hence, adsorption studies were conducted by varying two-factors: the velocity and pressure of the injected CO<sub>2</sub>. This

was done by injecting the same amount of CO<sub>2</sub> for all adsorbents. The variation of these two-factors allows us to estimate the flow and pressure of the injected CO<sub>2</sub> required reaching thermodynamic equilibrium inside the column. Powder XRD patterns were obtained using a Panalytical X-Pert high score plus diffractometer in the range 3° - 70° 2θ, at a scanning rate of min<sup>-1</sup> and employing Cu Kα filtered radiation.

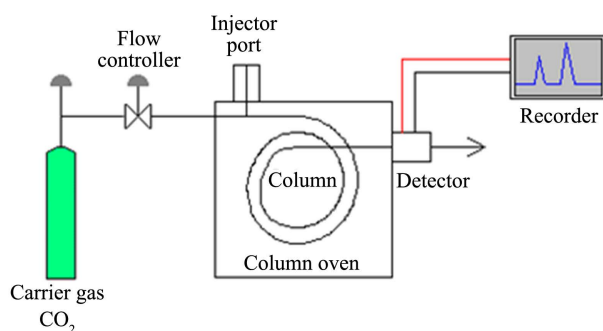
## 2.1. Adsorbents Characterization

**Table 1** shows the chemical composition (wt%) data of the selected three samples. The data indicate that the percentage of SiO<sub>2</sub> in clay and Triassic sandstone samples was relatively high. This is consistent with the presence of quartz as shown by XRD [**Figure 2(a)**]. The higher concentration of Na ion in the evaporate sample confirmed the presence of the halite. The percentage of the K<sub>2</sub>O in the clay and Triassic sandstone show that the illite is the major compound in both samples.

**Figure 2** presents the XRD patterns of three powder samples. As illustrated by this figure, the clay sample [**Figure 2(a)**] essentially comprises illite (10 Å) and kaolinite at 7.16 Å; the associated minerals are dolomite (2.88 Å) and quartz (3.34 Å). X-ray diffraction analysis of the evaporate sample shows the presence of halite at 2.82 Å and 1.99 Å [**Figure 2(b)**]. The Triassic sandstone samples are composed of illitic and kaolinitic clay associated to quartz [**Figure 2(c)**].

The SEM analysis (**Figure 3**) exhibits the morphology of the three soils. The SEM imaging shows that the particle morphology is laminated. This is due to the clay fraction in the sample represented by the layers of argillaceous form. In the case of Jurassic evaporates, the particles have a spherical form with very small compared to the others samples.

In **Table 2**, we provide the textural characteristics of these different materials obtained with the Nitrogen adsorption technique. The specific surface area and the total pore volume are the most important characteristics of adsorbents. For all samples, the SBET is relatively lower and the clay sample has the highest specific surface area. The total pore volumes of these samples are comparable.



**Figure 1.** Schematic diagram of the experimental set-up.

**Table 1.** Chemical composition of different adsorbents.

Samples	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	CaO	Fe <sub>2</sub> O <sub>3</sub>	Na <sub>2</sub> O	K <sub>2</sub> O	MgO	TiO <sub>2</sub>	I. Lo
Clay	52.18	11.96	8.91	5.09	0.20	2.82	6.89	0.03	9.4
Triassic sandstone	49.19	18.33	1.62	9.26	0.72	3.66	2.98	0.04	15.5
Jurassic evaporates	3.50	0.93	3.73	0.67	19.42	0.15	0.62	0.03	67

**Table 2.** Textural characteristics of different adsorbents.

Adsorbents	Specific surface BET (m <sup>2</sup> /g)	Total pore volume (cm <sup>3</sup> /g)
Clay	10.97	0.041
Triassic sandstone	6.09	0.047
Jurassic evaporates	4.04	0.036

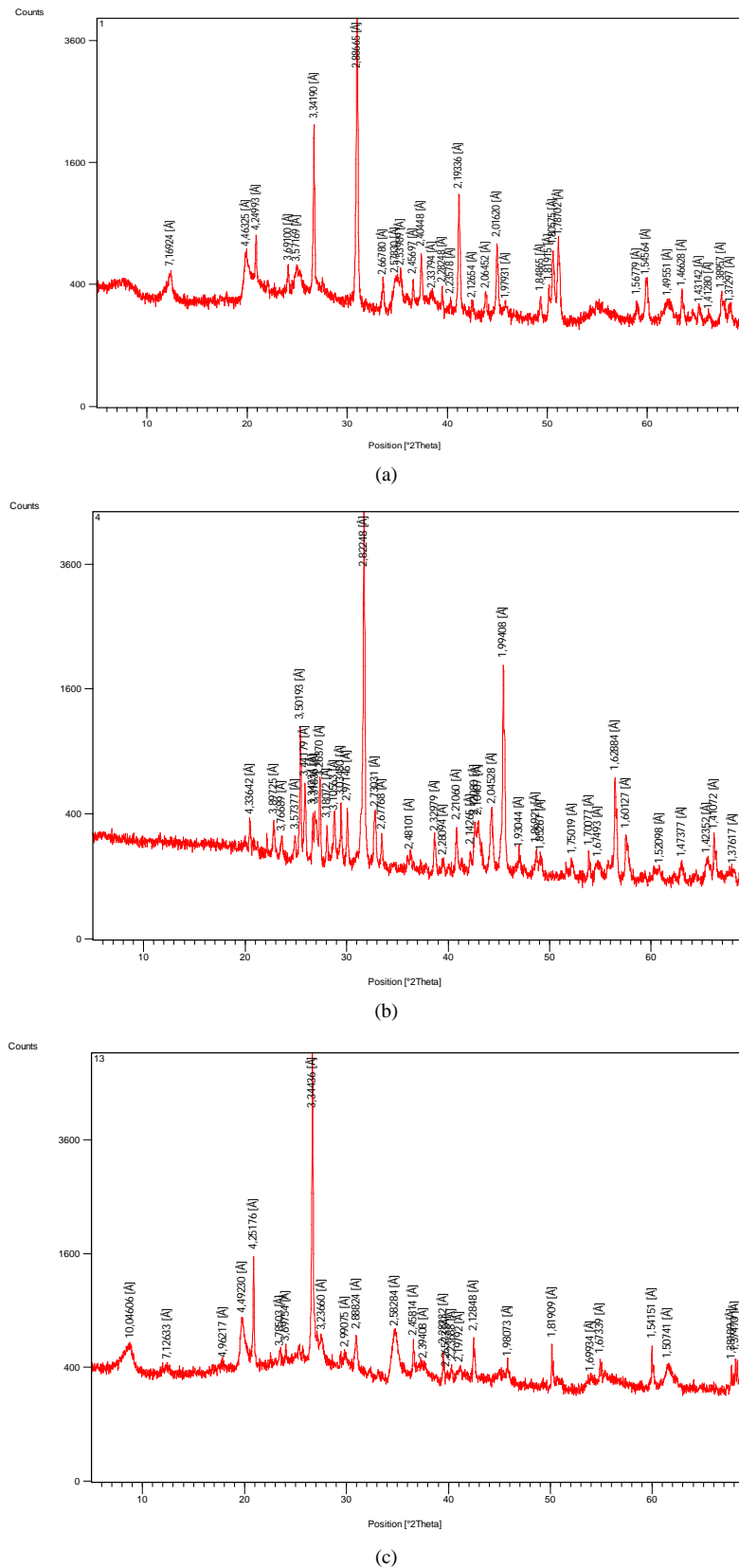
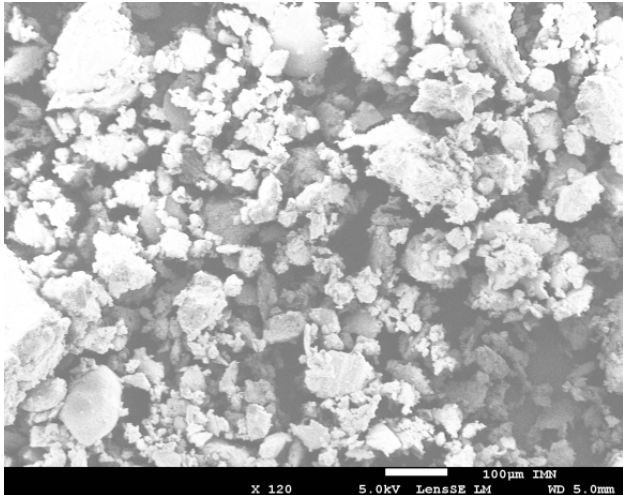
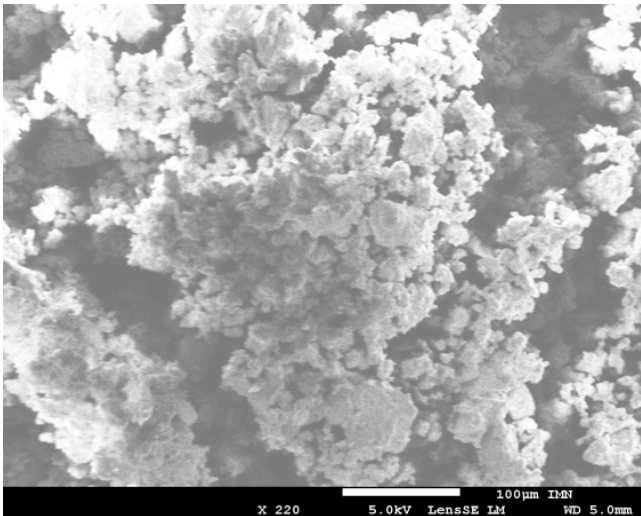


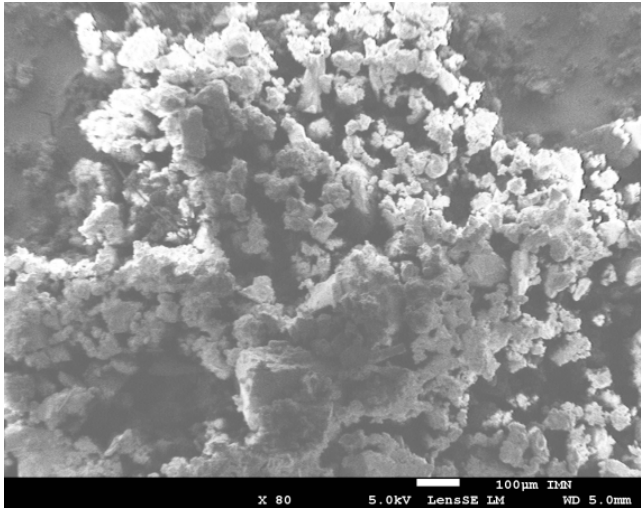
Figure 2. X-ray diffraction patterns of cuttings samples of (a) Clay; (b) Jurassic evaporates and (c) Triassic sandstone.



(a)



(b)



(c)

**Figure 3.** SEM images of (a) Clay; (b) Jurassic evaporates and (c) Triassic sandstone.

## 2.2. Operating Mode

In this study, a gas chromatograph series IGC 10 M was used to study the adsorption of CO<sub>2</sub> on the following adsorbents: clay, Triassic sandstone and Jurassic evaporate. It is worth noting that the most important difference between these samples is the particle size and the outer surface.

After filling with a given mass of adsorbate, the adsorption column is conditioned with a stream flow of CO<sub>2</sub> and heated to a temperature of about 120°C during 24 hours to remove any residual moisture. Then, the system is cooled to the ambient temperature. CO<sub>2</sub> is introduced directly into the chromatograph through a manual injection valve (Figure 1).

We balance the katharometer at each injection; check the flow rates of the gas in the reference column and that adsorbed. Then, a definite amount of CO<sub>2</sub> is adsorbed for a given injection pressure, depending on the flow rate value and injection temperature, an electrical signal in the form of a chromatographic peak is obtained on a recording paper.

At this stage, one can detect the coordinates in each chromatogram point using a Matlab program based on the trapezoidal method.

## 3. Results and Discussion

### 3.1. Choice of Equilibrium Conditions

The adsorption experiments were conducted to estimate the gas flow rate and the pressure of CO<sub>2</sub> injected at the inlet in order to reach thermodynamic equilibrium inside the column. For this purpose, we inject a fixed amount of CO<sub>2</sub> in a column filled with a mass  $m_b$  of adsorbent, at a velocity  $V_{inj}$  and a specific temperature  $T_{inj}$ . Then, we vary the flow vector gas,  $D$ , setting the pressure of the injected CO<sub>2</sub> from the inlet. Table 3 summarizes the equilibrium conditions inside the column for each adsorbent. The adsorption experiments were conducted to estimate the gas flow rate and the pressure of CO<sub>2</sub> injected at the inlet in order to reach thermodynamic equilibrium inside the column. For this purpose, we inject a fixed amount of CO<sub>2</sub> in a column filled with a mass  $m_b$  of adsorbent, at a velocity  $V_{inj}$  and a specific temperature  $T_{inj}$ . Then, we vary the flow vector gas,  $D$ , setting the pressure of the injected CO<sub>2</sub> from the inlet. Table 3 summarizes the equilibrium conditions inside the column for each adsorbent.

### 3.2. Adsorption Isotherms

For each pair CO<sub>2</sub>/adsorbent, we have made several injections at different temperatures. The obtained experimental results are shown in Table 4.

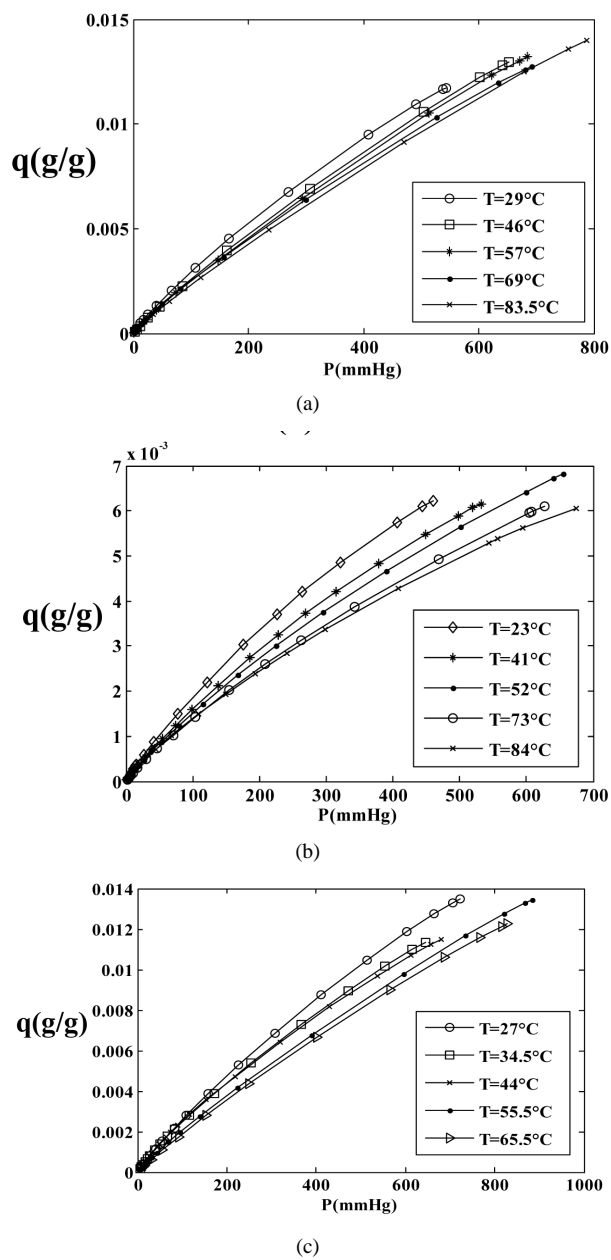
The study of Figure 4 shows that all the CO<sub>2</sub> adsorption isotherms on the selected adsorbents have the same shape and are of type I according to the classification of BDDT. Therefore, we can conclude that basically a

**Table 3.** Equilibrium conditions inside the column.

Adsorbent	D (m <sup>3</sup> /h)	P <sub>CO<sub>2</sub></sub> (bar)
Clay	0.00296	10
Triassic sandstone	0.00311	10
Jurassic evaporates	0.00302	10

**Table 4.** Results obtained from the isotherms of selected adsorbents.

Adsorbent	Temperature T (°C)	Isothermal type	Exothermicity	Adsorption capacity ( $q_m \times 10^3$ (g/g))	Reference	Smoothing model
Clay	29 - 83.5	I	+	15	[10]	Freundlich
Triassic sandstone	27 - 65.5	I	+	14	-	Langmuir and Freundlich
Jurassic evaporates	23 - 84	I	+	7	-	Freundlich



**Figure 4.** Adsorption isotherms of (a) CO<sub>2</sub>/Clay; (b) CO<sub>2</sub>/Triassic sandstone and (c) CO<sub>2</sub>/Jurassic evaporate at different temperatures.

monolayer adsorption takes place for all the adsorbents in the fixed operating conditions.

Furthermore, the isotherms show no flat curves, indicating that the adsorption sites are not saturated in the range of the introduced amount of CO<sub>2</sub>. In all cases, the largest adsorption capacity occurs at the lowest temperature (room temperature) and decreases with the increase of the injection temperature. This is obvious since we are dealing with an exothermic adsorption phenomenon.

### 3.3. Modeling of Adsorption Isotherms

Langmuir and Freundlich models are extensively used to model adsorption isotherms of CO<sub>2</sub> on different adsorbents [11]-[13].

The Langmuir model is used to calculate the maximum adsorbed amount  $q_m$  to form the monolayer as well as

the adsorption constant  $K_L$  [14] [15]. These parameters are determined using the linearization of the model [equation (1)] by plotting  $1/q$  vs.  $1/P$ .

The linear form of Langmuir model equation allows us to determine the parameters of this model (*i.e.*  $q_m$  and  $k_L$ ). This model is given by the following equation [16] [17]:

$$\frac{1}{q} = \frac{1}{q_m k_L P} + \frac{1}{q_m} \quad (1)$$

When we plot  $1/q$  as a function of  $1/P$ , one can obtain a straight line with a slope  $1/q_m k_L$  that intercepts  $1/p$ -axis at  $1/q_m$ . Then, the two-parameters of this model can be deduced.

It is important to note that Langmuir model is a good representation of adsorption isotherms of type I.

The Freundlich model parameters  $n$  and  $K$  are also determined by the linearization of the empirical model [Equation (2)] by plotting  $\log(q)$  as a function of  $\log(P)$ . Freundlich model is represented by the following relationship:

$$\log(q) = \log(K) + \frac{1}{n} \log(P) \quad (2)$$

where  $K$  is the Freundlich constant which is mainly related to the maximum adsorption capacity and  $n$  a constant characterizing the interaction between adsorbate and adsorbent. In general, this model is valid for the monolayer adsorption on heterogeneous surfaces, where the adsorption sites are different in nature [17] [18].

By plotting  $\log(q)$  as a function of  $\log(P)$ , one can get a straight a line with a slope  $1/n$  that intercepts  $\log(P)$ -axis at  $\log(K)$ .

The analysis of **Table 5** shows that the Langmuir model describes correctly the adsorption isotherms of CO<sub>2</sub> on clay for all fixed temperatures with a correlation coefficient  $R^2$  between 0.9995 and 0.9998. The high values of the correlation coefficients obtained in the case of CO<sub>2</sub> adsorption on clay are in agreement with the basis of Freundlich model, involving surface heterogeneity.

It is important to highlight that above 46°C, the maximum capacity  $q_m$  predicted by the Langmuir model is systematically lower than the adsorbed amounts [ $12.0482 \times 10^{-3}$  (g/g)]. However, the capacity  $q_m$  must be greater than or equal to the adsorbed quantities calculated from the isotherm curves. Although, the correlation coefficients are satisfactory (between 0.9971 and 0.9996), the values of  $q_m$  are meaningless.

The Freundlich model parameters  $n$  and  $K$  are also provided (**Table 6**). As it is well known, lower values of

**Table 5.** Parameters of langmuir and freundlich for clay.

Temperature (°C)	Langmuir			Freundlich		
	$q_m \times 10^3$ (g/g)	$K_L \times 10^3$	$R^2$	$K \times 10^5$	$n$	$R^2$
29	9.3458	4.5379	0.9994	5.2275	1.1533	0.9995
46	12.0482	2.7741	0.9996	3.9166	1.1102	0.9997
57	6.3694	5.6810	0.9994	4.0198	1.1207	0.9998
69	4.6083	10.1539	0.9971	5.8155	1.2142	0.9997
83.5	6.0976	5.4758	0.9995	3.7484	1.1206	0.9998

**Table 6.** Parameters of langmuir and freundlich for the triassic sandstone.

Temperature (°C)	Langmuir			Freundlich		
	$q_m \times 10^2$ (g/g)	$K_L \times 10^3$	$R^2$	$K \times 10^5$	$n$	$R^2$
27	2.17	1.4157	0.9998	4.1884	1.1292	0.9989
34.5	0.99	3.4877	0.9992	4.6308	1.1656	0.9994
44	1.08	3.1912	0.9998	4.6642	1.1675	0.9978
55.5	1.61	1.5538	0.9998	3.2845	1.1213	0.9994
65.5	2.78	0.7611	0.9998	2.7674	1.0971	0.9951



$n$  imply a higher heterogeneity of sites [19]. In our case,  $n$  is higher than 1 which implies that heterogeneity of sites is lower. In addition, the  $K$  values vary slightly with temperature.

From **Table 6**, it comes out that the Langmuir model describes adequately the experimental data of adsorption of CO<sub>2</sub> on the Triassic sandstone for all the tested temperatures with a correlation coefficient  $R^2$  between 0.9992 and 0.9998. Therefore, the experimental adsorption isotherms can be linearized according to the Langmuir model. In addition, the CO<sub>2</sub> adsorption isotherms of the Triassic sandstones can be correctly described by the Freundlich model. The obtained correlation coefficients imply a high surface heterogeneity. Furthermore, the value of  $n$  is greater than 1 indicating that the heterogeneity of sites is low. Results show also that  $K$  values are strongly subordinate with temperature and that adsorption sites are not energetically homogeneous.

It is worth noting that for a temperature above 27°C, the maximum capacity  $q_m$  predicted by the Langmuir model is below the maximum capacity  $q_m$  for the same temperature obtained from the adsorption isotherms. Thus,  $q_m$  values seem to be coherent and meaningful. According to **Table 7**, the Langmuir model describes well the experimental data. It reflects a localized adsorption on homogeneously-distributed sites. The Freundlich model describes appropriately the adsorption isotherms for the couple CO<sub>2</sub>/(Triassic evaporates) for different temperatures values. Moreover, the changes in the Langmuir parameters are not regular with temperature.

It is important to note that for all temperatures, the maximum adsorbed amounts of CO<sub>2</sub> (*i.e.*  $q_m$ ) predicted by the Langmuir model are systematically lower than the adsorbed amounts corresponding to an injected amount of CO<sub>2</sub> equal to 0.42 cm<sup>3</sup>. However, the values of  $q_m$  should logically be higher or equal to the quantities adsorbed when plotting isotherms [ $7 \times 10^{-3}$  (g/g)]. Thus, the obtained values of  $q_m$  are meaningless, even if the Langmuir curves are satisfactory.

Then, we can conclude that the Langmuir model does not allow us to describe correctly the adsorption isotherms of CO<sub>2</sub> on the Jurassic evaporate. In addition, the values of  $K_L$  indicate a low affinity of CO<sub>2</sub> on evaporate with relatively-homogeneous sites.

### 3.4. Thermodynamics Adsorption Study

In order to determine the adsorption nature for each adsorbent, we have calculated the enthalpy of adsorption based on the Clausius-Clapeyron equation.

$$\frac{\partial \ln(P)}{\partial \left(\frac{1}{T}\right)} = \frac{\Delta H_{ads}}{R} \quad (3)$$

Obviously, the isosteric enthalpy of adsorption  $\Delta H_{ads}$  is an important thermodynamic property in gas-solid adsorption problems. Then, it is necessary to draw the isosteric isotherms obtained at different temperatures. To this end, we have plotted the variation of  $\ln(P)$  as a function of  $1/T$  [20]. These results are not shown here for the sake of brevity. The slopes of these isosteres represent the adsorption enthalpy values divided by the ideal gas constant  $R$ .

We note that the curves  $\Delta H_{ads}$  as a function of  $q$  for all adsorbents (Clay, Triassic Sandstone and Jurassic evaporates) [21], not shown here for the sake of brevity, present negative values which confirm the exothermic nature of the adsorption phenomenon. In addition, the comparison between enthalpy adsorption values against available literature values are within the magnitude of the physical adsorption [20] [22]. We note also that the variation of isosteric enthalpy is small for clays and evaporates, showing that the heterogeneity of their sites is low.

In **Table 8**, the adsorption enthalpies of the different three couples studied here are depicted. In terms of CO<sub>2</sub> adsorption on clay, the average isosteric heat of adsorption is equal to 3.2904 kJ/mol. Variations in enthalpy as a function of the adsorbed amount are quite small for this material, suggesting that the heterogeneity of its surface is low, for the Triassic sandstone, the enthalpy of adsorption appears as an increasing function of the adsorbed amount or recovery rate and the isosteric heat of adsorption is equal to 6.5007 kJ/mol. For Jurassic evaporates, one can see that the enthalpy of adsorption decreases when the amount adsorbed increases. This can be explained by the fact that the adsorption of molecules on the first layer is on the first parts of the surface having the highest interaction energy. The adsorption of the molecules results in heat generation with an average isosteric adsorption heat equal to 5.6990 kJ/mol.

**Table 7.** Parameters of Langmuir and Freundlich for the Liassic evaporate.

Temperature (°C)	Langmuir			Freundlich		
	$q_m \times 10^3$ (g/g)	$K_L \times 10^3$	$R^2$	$K \times 10^5$	$n$	$R^2$
23	4.7847	5.8064	0.9994	3.3368	1.1566	0.9992
41	5.1282	4.4562	0.9997	2.7794	1.1464	0.9990
52	4.9751	4.3223	0.9996	2.6512	1.1525	0.9988
73	3.4130	6.2768	0.9992	2.5773	1.1663	0.9995
84	3.3003	7.1403	0.9993	3.1605	1.2214	0.9985

**Table 8.** Adsorption enthalpies for different adsorbents.

Adsorbents	$-\Delta H_{ads}$ (kJ/mol)
Clay	3.2904
Triassic sandstone	6.5007
Jurassic evaporates	5.6990

### 3.5. Comparative Study of Adsorbents

In this section, we aim to develop a comparative study between the adsorbents in order to choose the most efficient one for the adsorption of carbon dioxide CO<sub>2</sub>.

Based on the previous discussions, the CO<sub>2</sub> adsorption on different materials is exothermic. Indeed, the temperature plays an important role as it influences the adsorption capacity by affecting the amount of the adsorbed CO<sub>2</sub> molecules. It has been observed that the number of molecules in the column at the equilibrium decreases with temperature. Therefore, the best adsorption capacity of CO<sub>2</sub> is obtained at a low temperature, (*i.e.* for a temperature close to room one). The adsorbed amount of CO<sub>2</sub> on different adsorbents at low temperatures is illustrated in **Table 9**.

Increasing the capacity of adsorption of various adsorbents is in the following order:  $q_{\text{clay}}(15) > q_{\text{Triassic sandstone}}(14) > q_{\text{Jurassic evaporates}}(7)$ . Moreover, the largest adsorption capacity was found with clay due to its larger surface area (10.97 m<sup>2</sup>/g) followed by the Triassic sandstone (6.09 m<sup>2</sup>/g). The highest percentages of SiO<sub>2</sub> group in these two-adsorbents promote a good adsorption of CO<sub>2</sub>.

Hence, the choice of an adsorbent depends on several factors such as:

- Chemical composition of the adsorbent surface;
- The textural characteristics of the adsorbent (specific surface area, pore size distribution, connected micro-porous...);
- The operating conditions of adsorption.

## 4. Conclusions

This study was devoted to comparing the CO<sub>2</sub> adsorption by an adsorbent from El Borma field located in southern Tunisia and to selecting an efficient adsorbent suitable for storage. A thermodynamic study of CO<sub>2</sub> adsorption on different adsorbents (Clay, Triassic sandstone, Jurassic evaporates) was performed.

The analysis of the adsorption isotherms allowed us to conclude that the isotherms are of type I according to the classification of BDDT resulting in a monolayer adsorption. In addition, the isotherms show us the absence of flat curves, indicating that the adsorption sites are not saturated in the range of the considered amount of CO<sub>2</sub> adsorbed. The shape of the isotherms reflects a constant affinity of CO<sub>2</sub> adsorption on different materials.

Moreover, the two-models of Langmuir and Freundlich are appropriate for describing the phenomenon of CO<sub>2</sub> adsorption for these materials. The clay and Triassic sandstone have a higher adsorbent capacity of CO<sub>2</sub> compared to Jurassic evaporate. Furthermore, the adsorption of CO<sub>2</sub> on the selected material is exothermic. Indeed, the temperature affects the adsorption capacity. The number of molecules in the column at equilibrium

**Table 9.** Amount of carbon dioxide adsorbed on different adsorbents.

Adsorbents	Temperature (°C)	Q × 10 <sup>3</sup> (g/g)
Clay	29	15
Triassic sandstone	27	14
Jurassic evaporates	23	7

decreases with the increase of temperature. Therefore, the best adsorption capacity of carbon dioxide is obtained at low temperature.

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## Nomenclature

- D—Flow rate [m<sup>3</sup>/h];  
P<sub>CO<sub>2</sub></sub> —CO<sub>2</sub> injection pressure (bar);  
V<sub>inj</sub>—injection velocity [m/s];  
T<sub>inj</sub>—Injection temperature (°C);  
T—Ambient Temperature (°C);  
q—Adsorbed amount (g/g);  
q<sub>m</sub>—Maximum adsorbed amount (g/g);  
P<sub>CO<sub>2</sub></sub> —Injection pressure of CO<sub>2</sub> (bar);  
K<sub>L</sub>—Constant for a given adsorbate at a particular temperature;  
n—Constant for a given adsorbent at a particular temperature;  
R<sup>2</sup>—Correlation Coefficient;  
R—Ideal gas constant (J.K<sup>-1</sup>.mol<sup>-1</sup>);  
ΔH<sub>ads</sub>—Isosteric enthalpy of adsorption (KJ/mol);  
BDDT—Brunauer, Demming & Teller Classification;  
BET—Brunauer-Emmett-Teller, Measurement technique of the specific surface area of a material.

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