

# Amplify and Forward Relaying Systems for Collocated Antennas

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## Abstract

Cooperative relaying for a system that consists of different configurations of a collocated and uniform linear antenna is analyzed. The amplify-and-forward relaying (AF) and selection combining (S-AF) schemes based on maximal ratio combining (MRC) method for single- and multi-relay are investigated. In this study, the bit-error-rate (BER) expression for collocated and uniform linear antenna in cooperative communication system over flat Rayleigh fading channel is derived. The result for 3-element collocated antennas (tripole) shows improvement in performance over dual-polarized antennas. Also increasing number of tripole antenna does not add improvement.

## Keywords

Cooperative Communications, Fading Channels, Relay, Antennas

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## 1. Introduction

Relay systems have been widely investigated in wireless communications as a way to overcome deep fading and therefore enhance signal quality in multi-path fading channels. In relaying network we have a two-hop link where the signal is transmitted in the first hop from a source to a relay node and in the second hop the signal at the relay node is retransmitted to the destination. At the same time, the source will transmit another copy of the signal directly to the destination. Therefore, the signal is transmitted from the source directly and via a relay node, so, the destination will receive the transmitted signal from two links referred as source-relay-destination and source-destination link. Now the signal received at the relay is forwarded to the destination by implementing two schemes known as amplify forward (AF) and decode forward (DF) [1]-[3]. In AF, the received signal at relay is amplified and re-transmitted. In DF, the received signal at relay is decoded then retransmitted again to destination. Earlier research was focused on employing single- and multi-antenna system for cooperative diver-

sity technique to exploit fading channels [3] [4]. In [3], the symbol error probability was derived for dual hop with single antenna in Rayleigh and Nakagami  $m$ -fading channels and the outage performance of communication system was investigated for AF and DF relaying network. Cooperative communication for a multi-relay network with multiple-input multiple-output network to exploit spatial diversity is investigated in [4]. Here, the relays and users cooperate in sharing information which in turn increases capacity and coverage area of wireless communications. Other techniques utilizing relays equipped with multi-antennas and multi-relay network are investigated where an infrastructure-based relaying deploying multi-antennas on a relay is presented in the work of Adinoyi *et al.* [5]. To decrease number of relay nodes and thus reducing cost, a single antenna is deployed at source and destination while multi-antennas are fixed on receiver side of relays. The receiver criterion is based on threshold relaying with MRC and selection combining. Also cooperative communication is studied when relay selection scenario applied for the best relay link. It was shown that selection relaying can achieve same diversity order as AF [6]-[8]. Furthermore, deploying multi-antennas at the source or relays receiver side shows improvement as number of antennas increased from 1 to 2 for high and low SNR but increasing antennas more than 2, did not add significant improvement in performance at high SNR [9] [10].

Since future wireless system trends require wireless terminals small in size, the advantage of using multiple antennas at a relay node will be limited by the space separation between antennas and thus correlation of wireless terminals will affect the system performance. In this paper the study of cooperative communication is applied for collocated antennas known as “vector antenna” (VA) implemented at a relay node over independent and identically distributed Rayleigh fading channels. Vector antenna can independently detect or excite all six EM field components enabling the communication system to access additional signaling dimensions, which may enhance performance in the same way as antenna arrays [11]. These extra dimensions can provide additional diversity to combat signal fading, allow the system to spatially leverage bandwidth by transmitting multiple separable signals in the same bandwidth, and improve the suppression of interference in a multiuser environment. Also, “tripole” antenna that consists of three mutually-orthogonal dipoles by Andrew *et al.* [12] have shown through simulation, that this antenna improves on the capacity of scalar and dual-polarized antennas for a simple propagation example involving a line-of-sight component and one reflected path. The end-to-end performance for a relay network employing vector and ULA antennas based on MRC are investigated and using AF and selection schemes and an expression for bit error rate for BPSK is derived. Since we are investigating the advantage of collocated antennas in relay network, AF and selection schemes are selected.

The organization of this paper is as follows: in Section 2 the system model is introduced for VA and ULA in a relay network and the output SNR is analyzed. In Section 3 the BER analysis for AF and S-AF schemes is presented. Finally, simulation of the system presented is compared with theoretical values of the equation derived.

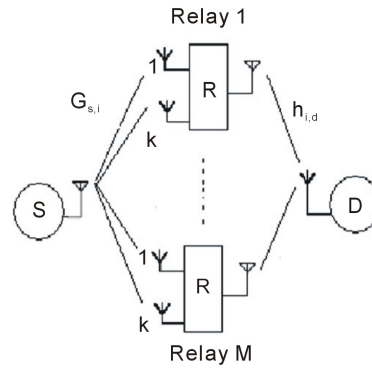
## 2. System Model

BPSK modulation is considered for a relay communication network that consists of two-hop channel as shown in **Figure 1**. In the first hop signals are transmitted from a single linear antenna at the source to the receiver side of relay node and in the second hop the received signal is transmitted from the transmitter side of relay node to the destination. The receiver side of the relay node is equipped with a vector antenna and the transmitter side with a uniform linear antenna. The source and destination nodes will use a single linear antenna. The channel assumed to be flat fading slowly time varying and the direct link from source to destination is considered only in S-AF.

For a single vector antenna at the receiver side of relay node, each arriving multipath component is a two-dimensional vector  $R(t)$ , consist of horizontally and vertically polarized components of the electric field. For narrowband sinusoidal signals, it is convenient to write the signal in terms of its complex envelope  $Z$ , where  $R(t) = \text{Re}\{\exp(j\omega ct)Z\}$ , and  $\omega c$  is the carrier frequency. For any polarized signal, the complex envelope can be written as

$$Z = Ae^{j\psi} \begin{bmatrix} \cos\alpha & \sin\alpha \\ -\sin\alpha & \cos\alpha \end{bmatrix} \begin{bmatrix} \cos\beta \\ j\sin\beta \end{bmatrix} \quad (1)$$

where  $A$ ,  $\psi$ ,  $\alpha$ ,  $\beta$  are the amplitude, phase, orientation angle, and ellipticity angle, respectively [13]. Since the signal is a function of the transmitted data, the amplitude, phase and polarization angles vary with time, and



**Figure 1.** Multi-relays system with vector antenna and ULA.

we write  $Z = Z(t)$ .

If the multipath component is reflected or scattered by an object in the far field, then the signal can be approximated as a plane wave at the receiver and suppose that the multipath component arrives at the sensor from the direction  $u_r$ ,

$$u_r = \begin{bmatrix} \cos\theta\sin\varphi \\ \sin\theta\sin\varphi \\ \cos\varphi \end{bmatrix} \quad (2)$$

nonconductive, homogeneous, and isotropic medium, the received signal can be modeled by [13]

$$Y(t) = \begin{bmatrix} \mathbf{E}(t) \\ \eta\mathbf{H}(t) \end{bmatrix} = B(\theta, \alpha)\mathbf{Z}(t) + N(t) \quad (3)$$

where  $N(t)$  represents thermal noise,  $\mathbf{E}(t)$  and  $\mathbf{H}(t)$  denote the three-dimensional complex envelopes of the electric and magnetic field vectors respectively at the receiver,  $\eta$  is the intrinsic impedance of the propagation medium, and

$$B(\theta, \varphi) = \begin{bmatrix} -\sin\theta & \cos\theta\cos\varphi \\ \cos\theta & \sin\theta\cos\varphi \\ 0 & -\sin\varphi \\ \sin\theta\cos\varphi & \sin\theta \\ \sin\theta\cos\varphi & -\cos\theta \\ -\sin\varphi & 0 \end{bmatrix} \quad (4)$$

The  $B(\theta, \varphi)$  vector antenna system will be used to detect information signal at receiver in the relay system of interest. The transmitted signal of a complex baseband signal of the form

$$S(t) = \sum_{j=1}^J b(j) \quad (5)$$

where  $b$  is a sequence of transmitted information bits. When  $S(t)$  is transmitted, the horizontally and vertically polarized components of each multipath component consist of  $S(t)$  with some amplitude and phase shift, so that  $Z(t) = ZS(t)$  for some fixed complex vector  $Z$ . Then the received signal can be written as

$$Y(t) = B(\theta, \varphi)ZS(t) + N(t) \quad (6)$$

with relay system notation, we can write the received signal from source to relay to be

$$Y_{s,i}(t) = \sqrt{E_s}B(\theta_{s,i}, \varphi_{s,i})Z_{s,i}S(t) + N_{s,i}(t) \quad (7)$$

where  $i = 1, \dots, M$  is number of relays and  $E_s$  is the transmitted power for the source and  $Z_{s,i}$  reflects the change in amplitude, phase, and polarization experienced by the fading component as it propagates from the

source to relay. The noise  $N_{s,i}(t)$  is zero-mean complex Gaussian vector with covariance  $\sigma^2 I$ . With abuse of notation we can write above equation at relay as

$$Y_{s,i}(t) = \sqrt{E_s} G_{s,i} S(t) + N_{s,i}(t) \quad (8)$$

where each of  $G_{s,i}$  consists of the appropriate  $L$  components of  $B(\theta_s, i, \varphi_s, i)$ . The components of the vector  $Z_{s,i}$  are modeled as i.i.d. zero-mean complex Gaussian random variables and therefore the elements of  $G_{s,i}$  are also zero-mean complex Gaussian random variables. The output of MRC at the relay is given by:

$$\gamma_{s,i}(t) = E_s G_{s,i}^+ S(t) R_n G_{s,i} \quad (9)$$

where  $\gamma_{s,i}$  is the SNR of the  $i^{\text{th}}$  relay. The noise  $R_n = I$  is white and assuming equal SNR on all branches. The received signal from  $i^{\text{th}}$  relay at destination

$$y_{d,i}(t) = \alpha_i G_{s,i}^+ G_{s,i} h_{d,i} S(t) + n_{i,d}(t) \quad (10)$$

where  $h_{i,d}$  is the channel gain from relay node to destination and the gain at the  $i^{\text{th}}$  relay can be written as

$$\alpha_i = \sqrt{\frac{E_i}{E_s |G_{s,i}|^2 + N_{s,i}}}, \quad i = 1, \dots, M \quad (11)$$

The noise  $N_{s,i}$  and  $n_{i,d} \in Ck$  are additive-white-Gaussian noise (AWGN) with zero mean and variance  $N_o$  and  $E_i$  is the transmitted power at the relay. At destination the receiver employ a maximal ratio combining algorithm and the received end-to-end SNR is given by

$$\gamma_{T,d} = \sum_{i=2}^m \frac{\frac{|G_{s,i}|^2 E_s |h_{i,d}|^2 E_i}{N_o}}{\frac{|G_{s,i}|^2 E_s}{N_o} + \frac{|h_{i,d}|^2 E_i}{N_o} + 1} = \sum_{i=1}^m \gamma_d \quad (12)$$

The output SNR at destination can be re-written as

$$\gamma_i = \frac{\gamma_{s,i} \gamma_{i,d}}{\gamma_{s,i} + \gamma_{i,d} + 1}, \quad i = 1, \dots, M \quad (14)$$

where  $\gamma_{s,i} = E_s |G_{s,i}|^2 / N_o$  is the SNR at  $i^{\text{th}}$  relay and  $\gamma_{i,d} = E_i |h_{i,d}|^2 / N_o$  is the SNR at destination from  $i^{\text{th}}$  relay. The SNR  $\gamma_{i,d}$  and  $\gamma_{s,i}$  are independent and identically distributed. Since the SNR is not mathematically tractable hence for high SNR it can be upper bounded by

$$\gamma_i = \frac{\gamma_{s,i} \gamma_{i,d}}{\gamma_{s,i} + \gamma_{i,d}}, \quad i = 1, \dots, M \quad (15)$$

To simplify the analysis, the noise is ignore at the relay gain. The output SNR of MRC at relay for tripole antenna is exponentially distributed and follows the Gamma distribution with probability density function pdf given by

$$P_{\gamma_{s,i}} = \frac{\gamma^{2k-1}}{\gamma^{2k} \Gamma(2k)} \exp\left\{-\frac{\gamma}{\gamma}\right\} \quad (16)$$

where  $k$  is number of tripole antennas at the relay and the pdf of SNR at destination is given by:

$$P_{\gamma_{i,d}} = \frac{1}{\gamma} \exp\left\{-\frac{\gamma}{\gamma}\right\} \quad (17)$$

Now using the results in [9] [10], the moment generation function of  $\gamma_{d,eq}$  is given by:

$$M_{eq}(s) = 3F_2\left(1, 2k, 1+k; \frac{2k+1}{2}, \frac{k+2}{2}; z\right) \quad (18)$$

where  $z = \frac{4\gamma}{\bar{\gamma}}$ .

### 3. Error Rate Analysis

#### 3.1. Amplify Forward (AF)

Assuming independent of  $\gamma$ , the bit error rate can be derived based on MGF approach in [14] that can be written as

$$P_e = \frac{1}{\pi} \int_0^{(c-1/c)} \prod_{i=1}^M M_{\gamma_{s,i}} \left( \frac{-\sin^2 \pi/c}{\sin^2 \varphi} \right) d\varphi \quad (19)$$

where  $c = 2$  for BPSK modulation and independent of  $\gamma_{d,eq}$ .

#### 3.2. Selective Amplify Forward (S-AF)

For S-AF only the best relay which contributes most to received SNR is chosen for re-transmission. The received SNR can be expressed as

$$\gamma^s = \frac{|G_{s,d}|^2 E_s}{N_o} + \max_i \frac{\frac{|G_{s,i}|^2 E_s}{N_o} \frac{|h_{i,d}|^2 E_i}{N_o}}{\frac{|G_{s,i}|^2 E_s}{N_o} + \frac{|h_{i,d}|^2 E_i}{N_o} + 1} \quad (20)$$

The received SNR for S-AF can be written as

$$\gamma^s = \alpha_o + \max_i \frac{\alpha_i \beta_i}{\alpha_i + \beta_i + 1} \quad (21)$$

where  $\alpha_o = |G_{s,d}|^2 E_s / N_o$ ,  $\alpha_i = |G_{s,i}|^2 E_s / N_o$  and  $\beta_i = |G_{i,d}|^2 E_i / N_o$ . At high SNR region, using the result in [6] for approximation of cumulative distribution function (CDF) of the received SNR for S-AF scheme, the CDF for tripole antenna is given by

$$F^s(\gamma^s) = \frac{\lambda_o^2 \prod_{i=1}^m (\lambda_i + \zeta_i)}{(m^2 + 3m + 2)} (\gamma)^{m+2} \quad (22)$$

where  $\gamma = \alpha_o + \frac{\alpha_i \beta_i}{\alpha_i + \beta_i + 1}$  and  $\lambda_o$  is exponentially distributed with pdf  $x \lambda_o^2 e^{-(\lambda_o x)}$ . Substituting Equation (22)

in  $P_e = \varepsilon \left\{ F \left( \frac{x^2}{c} \right) \right\}$  [[6], Equation (6)] and using  $\int_0^\infty x^{2n} e^{-px^2} dx = \frac{(2n-1)!!}{2(2p)^n} \sqrt{\frac{\pi}{p}}$ . The high SNR approximation can be written as

$$P_e^s \approx \int_0^\infty \frac{\lambda_o^2 \prod_{i=1}^m (\lambda_i + \zeta_i)}{m^2 + 3m + 2} \left( \frac{x^2}{c} \right)^{m+2} \frac{1}{\sqrt{2\pi}} e^{-\frac{x^2}{2}} dx = \frac{\lambda_o^2 \prod_{i=1}^m (\lambda_i + \zeta_i) (2m+3)!!}{4(m^2 + 3m + 2) c^{m+2}} \quad (23)$$

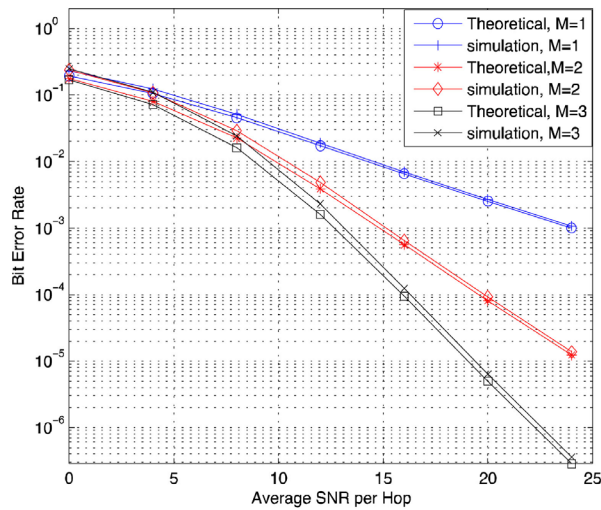
### 4. Simulation Results

In this section, simulation and theoretical results of cooperative communication for AF and S-AF schemes presented. We assume that the multipath components of the received signals are uniformly distributed on a sphere where the azimuth angle  $\theta_{s,i}$  are i.i.d. and uniform on  $\in [0, 2\pi]$ , and the elevation angles  $\varphi_{s,i}$  are i.i.d. with probability density function

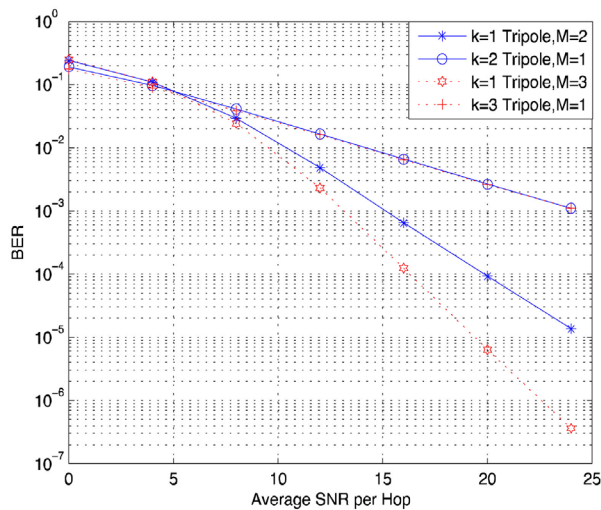
$$P(\varphi_{s,i}) = \begin{cases} \frac{1}{2} \sin(\varphi_{s,i}), & 0 \leq \varphi_{s,i} \leq \pi \\ 0, & \text{otherwise} \end{cases} \quad (24)$$

and the polarizations  $Z_{s,i}$  are i.i.d.  $CN(0, I)$ . The noise  $n(t)$  is spatially and temporally white and Gaussian (i.e.  $E[n(t)n^+(t+\tau)] = \sigma^2 I$ ). The fading channel is assumed to be a flat fading Rayleigh channel. The transmitted power for all participate scheme on each relay is  $E_s = E_t/M$ , where  $M$  is the relay number and total transmitted power  $E_t = E_i$ . In selective scheme, the transmitted power for each relay is  $E_s$ . The antenna setting in all simulation will be based on the following setting: the source, destination and transmitter side of the relay will employ ULA while the receiver side relay will have vector antenna that consist of either dual, tripole or 6-element antennas as specified in the figures below.

In **Figure 2**, the results are plotted for 1, 2 and 3 relays where each relay will assume a single tripole antennas. Simulation and theoretical BER are compared. The figure shows that as number of relays increase, BER will decrease and therefore increase of diversity gain. On the other hand the theoretical results came in a very close approximation to our simulation. In **Figure 3**, the results shows an increase in the number of tripole antennas on



**Figure 2.** BER for tripole antenna with multi-relays.



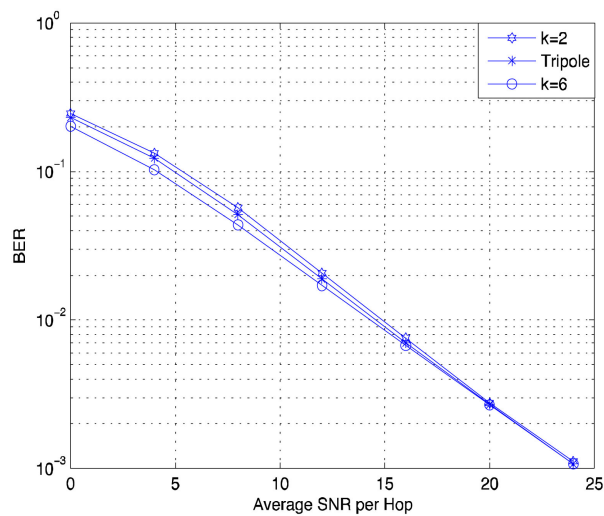
**Figure 3.** BER simulation for tripole antenna at single and multi-relays.

a relay did not add gain in diversity to the relay system while multi-relay network with single triple antenna would give us significant improvement.

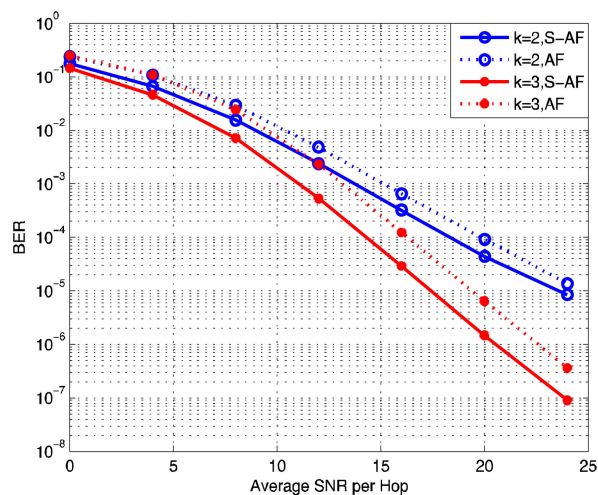
In **Figure 4**, simulation of 2, 3 and 6-element collocated antenna for one relay are compared. The results show that a 2 dB gain at low SNR region for 6 over 2 elements collocated antennas but no gain is noticed in the high SNR region. In **Figure 5**, selective relaying simulation for 2 and 3 relay network is presented. The relay with highest SNR is chosen where each relay is equipped with one tripole antennas. As the number of relays increased, diversity improve and on the same figure BER for selection is compared with all participate scheme. The results show that selection (S-AF) outperforms AF scheme in all cases considered.

## 5. Conclusion

The study of cooperative communication for collocated antennas setting employed at relay node and ULA at source and destination is investigated. Two schemes of relaying network known as AF and S-AF are presented and closed form BER for tripole antennas is derived. The theoretical and simulation results are compared for one- and multi-relay network. Results shows that tripole antenna outperformed the dual antenna case and the 6-



**Figure 4.** BER simulation for 2, 3 and 6 collocated antennas at single relay.



**Figure 5.** BER Simulation for selective vs AF for tripole and  $M = 2,3$  relay.

element vector antenna can add more gain in low SNR region over tripole case. Also increasing number of tripole antenna showing no gain is attained while increasing number of relays will enhance the receiver performance and achieve higher gain.

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