

Research on Numerical Simulation of 3D Leakage Magnetic Field and Short-circuit Impedance of Axial Dual-low-voltage Split-winding Transformer*

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ABSTRACT

It is difficult to accurately calculate the short-circuit impedance, due to the complexity of axial dual-low-voltage split-winding transformer winding structure. In this paper, firstly, the leakage magnetic field and short-circuit impedance model of axial dual-low-voltage split-winding transformer is established, and then the 2D and 3D leakage magnetic field are analyzed. Secondly, the short-circuit impedance and split parallel branch current distribution in different working conditions are calculated, which is based on field-circuit coupled method. At last, effectiveness and feasibility of the proposed model is verified by comparison between experiment, analysis and simulation. The results showed that the 3D analysis method is a better approach to calculate the short-circuit impedance, since its analytical value is more closer to the experimental value compared with the 2D analysis results, the finite element method calculation error is less than 2%, while the leakage flux method maximum error is 7.2%.

Keywords: Split-winding Transformer; Short-circuit Impedance; Field-circuit Coupled; Current Distribution

1. Introduction

Short-circuit impedance is the important technical parameter of power transformer [1,2]. The value of short-circuit impedance can influence the cost, efficiency, voltage regulation, mechanical strength, short-circuit current of transformer, so the deviation between measured value and rated value when the transformer leave factory is very strict. Split-winding transformer splits one winding into two ones, when one winding is short circuit it can increase the impedance, it's the effective and economy method to restrict the shot-circuit current. The application of split-winding transformer is used more and more widely following with the increase of unit capacity and system capacity [3-6]. So calculation of short-circuit impedance accurately in split-winding transformer is important in transformer design.

2D and 3D calculation model are established for a axial dual-low-voltage split-winding transformer which type is SFFZ10-88000 kVA/220 kV based on rational simplification and assumption. Apply field-circuit coupled method to compute and analysis the leakage magnetic field and short-circuit impedance, it could be used as the starting point for studying the load short circuit

current and distribution of high voltage parallel road current. At last, finite element, computing and experimental values are contrastive analyzed, then the finiteelement analysis is verified to be proper and more veracity.

2. Basic Parameter and Calculation Model of Split-winding Transformer

The structure diagram of axial dual-low-voltage splitwinding transformer is shown in **Figure 1**.

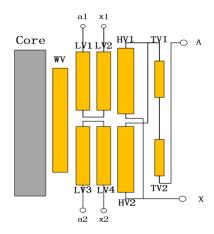


Figure 1. Structure diagram of winding.

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The arrangement of winding is core---balanced winding---low voltage winding---high voltage winding ---regulating winding. Low voltage winding break up into four equality rated capacity (LV1, LV2, LV3, LV4). High voltage winding adopt inlet line from central section, the two parts (HV1, HV2) are in parallel then connected in series with regulating winding (TV1, TV2). Regulating winding all accessing is maximum tap, reverse accessing is minimum tap. The low and high voltage winding of transformer are all Y connection, a balanced winding is needed to provide access of third harmonic current for enhancing waveform quality. The basic parameter of split-winding transformer is shown in **Table 1**. 3D calculation model of split-winding transformer is shown in **Figure 2**.

The assumption conditions are shown as follows:

- 1) The 1/2 model of whole transformer model is established in order to reduce the computational time;
- 2) The eddy currents and their influence on windings are neglected;
- 3) The currents in the windings are equally distributed along the cross section;
- 4) All field quantity sinusoidal variation with time, do not consider the high-order harmonic.

The diagram of external circuit that calculating the short-circuit impedance of transformer based on field-circuit coupled method is shown in **Figure 3**. **Figure 3(a)** shows the equivalent circuit diagram of crossing, **Figure 3(b)** shows the equivalent circuit diagram of semi-crossing.

Table 1. Basic Parameter of Split-winding Transformer.

Parameter	Value
Rated current of high voltage winding	109.95 A
Rated current of low voltage winding	2419.4 A
Rated current of regulating winding	219.9 A
Rated current of balanced winding	936.5 A
Turns of high voltage winding	773
Turns of low voltage winding	LV1,LV3(18),LV2,LV4(19)
Turns of regulating winding	40
Turns of balanced winding	64

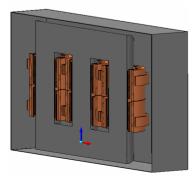
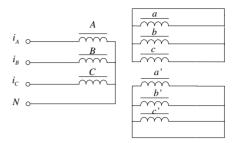
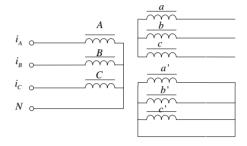


Figure 2. Model of split-winding transformer.



(a) Equivalent circuit diagram of crossing



(b) Equivalent circuit diagram of semi-crossing

Figure 3. Equivalent circuit diagram.

 i_A , i_B , i_C is the three-phase symmetrical current source with internal impedance at the secondary side of the transformer. A, B, C is the secondary winding consist of HV and TV. a, b, c is the primary winding consist of LV.

3. Calculation of Short-circuit Impedance

Calculation of short-circuit impedance percentage using analytical method can be governed by following equation:

$$U_{K} = \frac{49.6 f \cdot I_{N} W \sum D\rho K}{e_{t} H \times 10^{6}}$$
 (1)

where e_t is every turn potential, I_N is rated phase current of winding, W is total number of turns, H is average reactance height of coil, K is additional reactance coefficient, ρ is low-type coefficient, $\sum D$ is leakage magnetic area.

When calculate the short circuit impedance of transformer by the finite element method based on field-circuit coupled, energy of magnetic field stored in transformer is transformed from external source during setting up the magnetic field. Calculate the distribution of magnetic can obtain the energy of magnetic field stored in transformer [7,8]. When there is the current I_N in winding, energy of magnetic field W_m is:

$$W_m = \frac{1}{2}LI_N^2 \tag{2}$$

where W_m is magnetic field energy, L is inductance of winding, I_N is phase current.

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When resistive component of the short-circuit impedance can be ignored, the short-circuit impedance of corresponding rated current I_N is:

$$Z_{K} = \omega \cdot L = 2\omega W_{m} / I_{N}^{2} \tag{3}$$

where Z_K is short-circuit impedance (leakage reactance), ω is angular frequency of power source.

Percentage of short-circuit impedance is shown as:

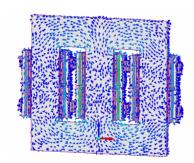
$$U_K = \frac{Z_K}{Z_N} = \frac{\omega L I_N}{U_N} = \frac{4\pi f W_m}{VA}$$
 (4)

Where U_K is percentage of short-circuit impedance, f is frequency, VA is capacity of single phase when transformer working under rated operating condition.

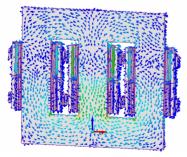
4. Analysis of Calculation Results

The short-circuit impedance of axial dual-low-voltage split-winding transformer is calculated and analyzed though analytical method, 2D and 3D finite element method. The distribution of leakage magnetic vector when the transformer is working under crossing and semi-crossing condition are respectively shown in **Figure 4(a)** and **Figure 4(b)**.

The comparison of results about the short-circuit impedance of split-winding transformer working under different conditions are shown in **Table 2**. In this table, low-up is LV1 and LV2 in the structure diagram, low-down is LV3 and LV4 in the structure diagram, Z_d is the short-circuit impedance of crossing, Z_B is the short-circuit impedance of semi-crossing.



(a) Leakage magnetic vector distribution of crossing



(b) Leakage magnetic vector distribution of semi-crossing

Figure 4. 3D leakage magnetic field distribution (rated tap).

Table 2. Short-circuit Impedance Results of Split- winding Transformer (%).

Calculation conditions		Calculation		Measured	Error/%
		Analytical	9.92		0.7
	Z_{d}	2D	9.76	9.85	0.9
		3D	9.83		0.2
RATE D		Analytical	18.5		0.27
	$Z_{\rm B}$ (high/low-up)	2D	18.59	18.55	0.22
TAP	(mgm/10 w up)	3D	18.63		0.43
		Analytical	18.5		0.16
	Z _B (high/low-down)	2D	18.65	18.47	0.97
	(mgm/10 W do Wil)	3D	18.63		0.87
		Analytical	10.08		0.5
	Z_{d}	2D	9.96	10.08	1.2
		3D	10.03		0.5
MA X		Analytical	18.87		0.53
	$Z_{\rm B}$ (high/low-up)	2D	18.86	18.77	0.48
TAP	(g.,, _I ,	3D	18.8		0.16
		Analytical	18.87		1
	Z _B (high/low-down)	2D	18.9	18.68	1.18
	,	3D	18.92		1.28
		Analytical	9.61		3.3
	Z_{d}	2D	9.87	9.94	0.7
		3D	10		0.6
MI N	_	Analytical	17.36		7.2
	$Z_{\rm B}$ (high/low-up)	2D	18.87	18.71	0.85
TAP	(8,1,1,1)	3D	18.82		0.59
	_	Analytical	17.36		6.5
	Z _B (high/low-down)	2D	18.78	18.57	1.13
		3D	18.82	- -	1.34

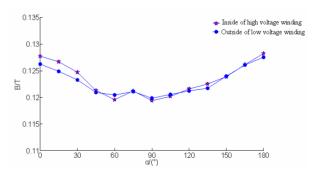


Figure 5. End winding magnetic flux density distribution along circle direction.

The distribution of magnetic flux density along circle direction of upper end of the winding under crossing condition is shown in **Figure 5**. The distribution of magnetic flux density is uneven along the circle direction of

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Table 3.	Current	calculation	of HV	parallel	branch	(-show
phase co	ntrast).					

Calc	ulation conditions	High voltage up/A	High voltage down/A
Rated tap	$Z_{\rm d}$	109.95	110.14
	$Z_B(high/low-up)$	111.02	-1.08
	$Z_B(high/low-down)$	-1.11	111.02
Max tap	Z_{d}	104.62	104.88
	$Z_B(high/low-up)$	108.62	-3.66
	$Z_B(high/low-down)$	-3.67	108.62
Min tap	Z_{d}	129.13	129.67
	$Z_B(high/low-up)$	120.92	8.46
	$Z_B(high/low-down)$	8.45	120.93

winding from the figure, the magnetic flux density in the core window is larger than that out of the core window.

The comparative analysis of the analytical method, 2D finite element method, 3D finite element method and measured values shows that the 3D finite element calculation value is more close to the measured value. Due to short-circuit impedance is decided by the value and regularity of distribution of leakage magnetic field, analytical method can not calculate the leakage magnetic accurately. 2D finite element method can not figure up the uneven of the distribution of magnetic field along the circle direction of winding. So the 3D finite element method is the best choice when calculating short-circuit impedance.

5. Analysis of Current Distribution

In this paper, the high voltage winding is connected in parallel, then series connected with regulating winding, current excitation is applied at high voltage side when calculating short-circuit impedance from **Figure 1**. The problem of current distribution is analyzed in different conditions, the calculation results of 3D finite element method are shown in **Table 3**.

Table 3 shows that the high voltage parallel branch current in crossing is not much different and equal division when in the three conditions; current in semi-crossing is different and distribution uneven. The reason for this phenomenon is that: under the semi-crossing, the two low voltage winding impedances are different in the up and down two parallel branches, and the magnetic field is mutual affected. At last, a circle flowing the two low-voltage winding is emerged to counteract the imbalance of impedance.

6. Conclusions

In this paper, an axial dual-low-voltage split-winding transformer is selected as the research object, calculation model of the equivalent circuit and the leakage magnetic field is established. Analytical method, 2D and 3D finite element method are used to calculate the short-circuit impedance of transformer in different conditions, then get the following conclusions:

- 1) The error of 3D finite element and measured values is in 2%. The maximum error of analytical method achieves 7.2%. The 3D finite element method is more accurate than the 2D one and analytical method.
- 2) The current distribution can be accurately obtained by 3D field-circuit coupled finite element analysis method though the analysis of current distribution of high voltage parallel branch, then the precise short-circuit impedance is gained. All of these can be the reference frame in the short-circuit design of split-winding transformer.

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